

Thermocouples

The most common problems associated with thermocouple sensing controls are:

1) Using the wrong type of thermocouple

Each instrument is calibrated to work with a particular thermocouple type. Connecting a 'K' thermocouple to a 'J' instrument will result in severe overshoot and probable heater damage.

2) Reversing of lead wires

Thermocouple leads are polarized. The red wire is always negative. Reversing leads will cause reverse reading at the instrument and loss of control.

3) Using the wrong extension wire

The correct thermocouple extension wire must be used. For example: type J thermocouple extension wire must be used with J thermocouples. Copper wire cannot be used. A mixture of copper and thermocouple wire creates extra thermocouple junctions which will cause unpredictable reading errors.

Refer to the following charts for proper physical identification:

Thermocouple Identification

TABLE 1 - Thermocouple Identification

ANSI TYPE	DESCRIPTION	COLOURS		JACKET
		POS+	NEG-	
J	Iron Constantan	White	Red	Black
K	Chromel Alumel	Yellow	Red	Yellow
T	Copper Constantan	Blue	Red	Blue
E	Chromel Constantan	Purple	Red	Purple
R	Platinum Rhodium 13%	Black	Red	Green
S	Platinum Rhodium 10%	Black	Red	Green
N	Nicrosil NISIL	Orange	Red	Brown

Thermocouple Output

TABLE 2 - Millivolt vs. Temperature

TEMP.		J (iron constantan) MILLIVOLTS	K (chromel alumel) MILLIVOLTS
°F	°C		
0	-18	-0.885	-
32	0	-0.000	0.000
100	38	1.942	1.520
212	100	5.268	4.095
300	149	7.947	6.092
500	260	14.108	10.560
700	371	20.253	15.178
1000	538	29.515	22.251
1250	677	37.688	28.146
1500	816	46.503	33.913
2000	1093	63.392	44.856

Thermocouple Extension Wire Resistance

Thermocouple wires have the resistance outlined in the following chart (Table 3). Resistances should be kept as low as possible. Increase the gauge of wire for long runs. Although modern instrumentation will accept an input impedance up to 100 ohms or more, the signal degrades and the instrument becomes more susceptible to external interference.

For long runs between sensing point and instrumentation of 50 meters (150 feet) or more, a transmitter should be considered.

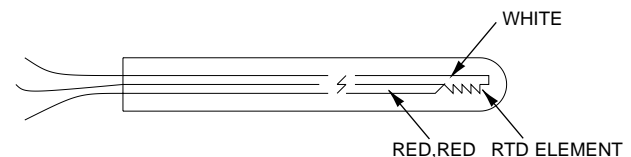
TABLE 3 - Loop Resistance (2 Wires)

CALIBRATION	Ohms per 33m (100')			
	8 GA	12 GA	14 GA	16 GA
JX Iron Constantan	2.15	5.42	8.63	13.71
KX Chromel Alumel	3.65	9.22	14.66	23.30
TX Copper Constantan	1.84	4.66	7.41	11.78
EX Chromel Constantan	4.36	11.01	17.51	27.83

CALIBRATION	Ohms per 33m (100')			
	18 GA	20 GA	22 GA	24 GA
JX Iron Constantan	21.80	35.69	55.11	87.66
KX Chromel Alumel	37.07	58.97	93.68	149.00
TX Copper Constantan	18.74	29.82	46.91	75.34
EX Chromel Constantan	44.27	70.43	111.90	178.00

RTD's

RTD's are available in 2, 3 and 4 wire construction. The most common (as shown) is 3 wire. With instrumentation designed to accept 3 wire RTD's, the second red wire is used in a circuit to calculate lead wire resistance. This resistance is automatically deducted from the sensor reading to eliminate potential errors.



RTD Output

TABLE 4 - 100Ω Platinum (.00385 Ω/Ω/°C) Resistance vs. Temperature

TEMP.		OHMS	TEMP.		OHMS
°F	°C		°F	°C	
-40	-40	84.27	302	150	157.31
-4	-20	92.16	392	200	175.84
32	0	100.00	482	250	194.07
68	20	107.79	572	300	212.02
122	50	119.40	662	350	229.67
212	100	138.50	752	400	247.04

Electrical Equations

Single phase relationships:

$$V = \sqrt{WR} = W/I = IR$$

$$RW/I^2 = V^2/W = V/I$$

$$I = V/R = W/V = \sqrt{W/R}$$

$$W = V^2/R = I^2R = VI$$

For current in electrically balanced three phase A.C. circuits:

$$I = \frac{W}{V(\sqrt{3})}$$

NOTE: For circuits wired in 3 phase delta, wattage may be reduced to 1/3 by rewiring to a 3 phase wye connection.

FIG. 1 - THREE PHASE DELTA CONNECTION

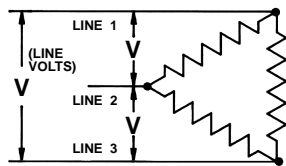


FIG. 2 - THREE PHASE WYE OR STAR CONNECTION

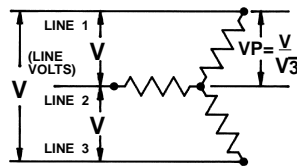


FIG. 3 - SPECIAL USE OF TWO POLE THERMOSTAT

Single phase circuit split with half of the current load across each thermostat contact.

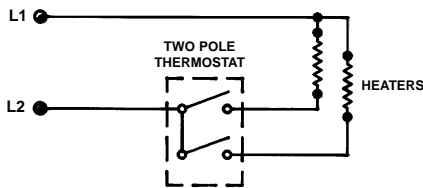


FIG. 4 - USE OF CONTACTOR (SINGLE PHASE)

Single phase circuit for conditions where the line current exceeds the thermostat rating and a contactor is added.

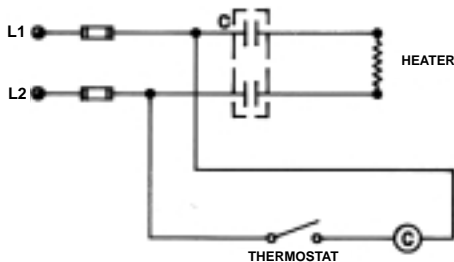


FIG. 5 - USE OF CONTACTOR (THREE PHASE)

Three phase circuit for conditions where the line current exceeds the thermostat rating and a contactor is added.

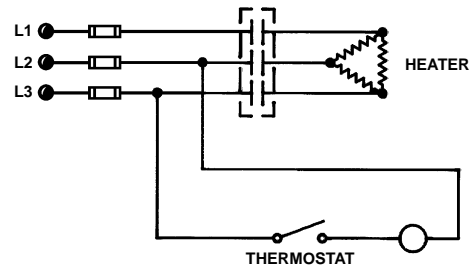


FIG. 6 - SERIES TO PARALLEL DELTA TRANSFORMATION

Special circuit with two thermostats and two contactors. When both contactors are closed, elements are wired in 3 phase parallel delta and circuit operates at full power. When only one of the contactors is closed, elements are wired in 3 phase series delta and the circuit operates at 1/4 power.

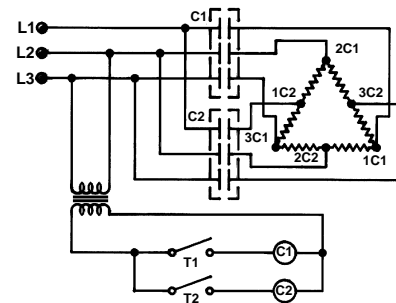
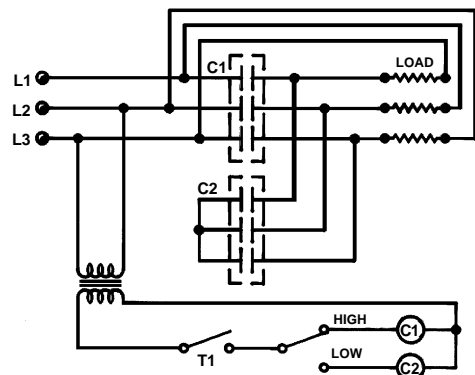


FIG. 7 - WYE TO DELTA TRANSFORMATION

Special circuit with two contactors, thermostat and two position switch.

When contactor 1 (C1) is closed, elements are wired in 3 phase delta and circuit operates at full power. When contactor 2 (C2) is closed, contactor 1 (C1) is opened, elements are wired in 3 phase wye and the circuit operates at 1/3 power. **CAUTION:** Contactors C1 and C2 must be mechanically interlocked in this configuration.

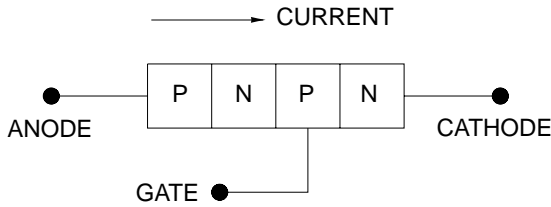


SCR'S, THYRISTORS, TRIACS & SSR'S

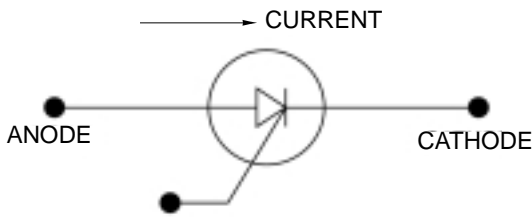
An SCR (Silicon Controlled Rectifier) as a component is one commonly used type of **thyristor**. Essentially, it consists of four layers of silicon which, in their normal state, are non-conductive.

The SCR can be made to conduct by applying a very small current to its "gate". This feature allows a combination of SCR's to have broad application, one of which is the switching of resistive loads characteristic of electric heating.

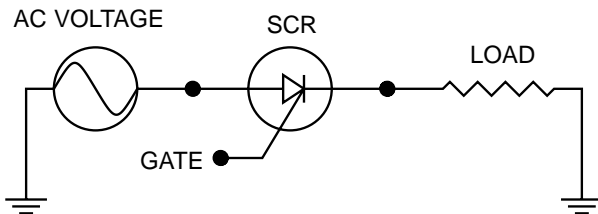
Diagrammatically, the SCR is represented as follows:



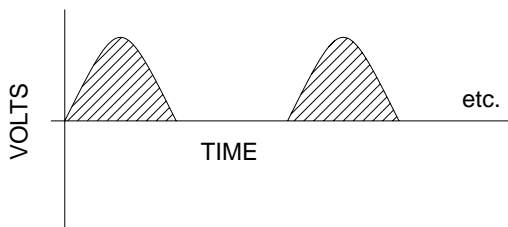
However, for electrical circuits, the SCR is depicted as follows:



If we connect a supply voltage and load (resistance) to the above circuit

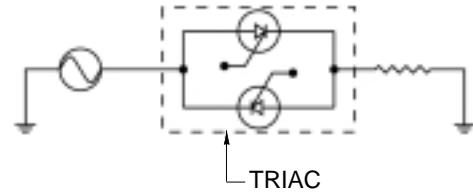


the single SCR will act as a half wave rectifier, and at best, it will only allow the positive (+) part of the AC voltage to reach the load.

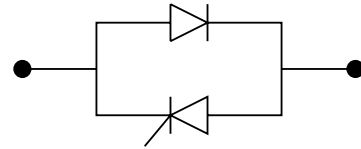


To allow the negative (-) part of the voltage waveform to get through to the load requires a second SCR of opposite polarity in parallel with the first.

For example, the circuit below will allow the full waveform or a part of it to reach the load. Two SCR's



combined in this fashion make up a **triac**. A triac is generally depicted as follows:



For single phase circuits, one triac will be sufficient to control the load. For three phase circuits, two triacs are normally used.

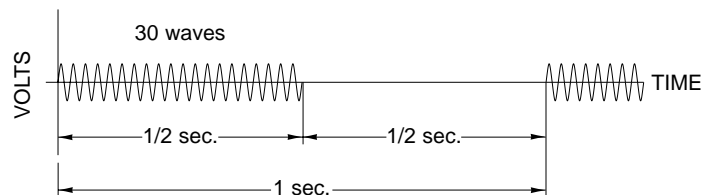
Controls are available which can apply a current to the gate at rapid intervals, blocking out some of the waveforms or a part of each waveform. The load output will then vary as a percentage of the blocked to the total cycles.

Two gate switching methods are in use to provide variable output from the load:

i) **Zero crossover fired** or **burst firing** where only full cycles of the voltage waveform are permitted to pass through the SCR to the load. Again, there are several variations as to how this can be done.

(a) **Fixed time base** where the cycle interval is built into the controller at the factory and the power is switched through only one "on" and one "off" cycle during that time. For example, if the time base is 1 second, at 60 cycles per second, any sequential number of the 60 voltage waves could be allowed to pass through to the load. At 50% demand the first 30 waves would pass and the last 30 would be blocked.

FIGURE 1 - Fixed (one second) time base at 50% output



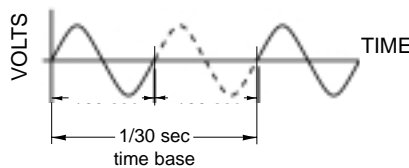
The SCR is equipped with circuitry (firing board) that will modify or proportion the "on" and "off" time during each subsequent cycle based on the amplitude of the temperature related signal it receives from an external controller.

Earlier SCR's employed fixed time bases up to 90 seconds. However, typical controls now in use tend to have time bases set at ten seconds or less. Most Caloritech™ SSR's have four second or one second fixed time bases.

SSR's (solid state relays) employ a similar method of control except that the time base is set by an external controller which signals the SSR's built-in firing circuitry when it should fire (conduct).

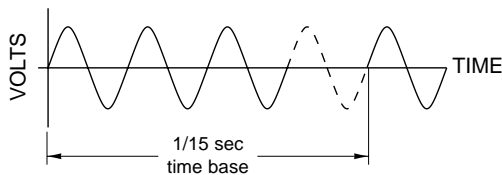
(b) **Variable time base** (also burst fired) where the time base depends on the demand. At 50% demand the time base would be 1/30 of a second or two cycles;

FIGURE 2 - Variable time base at 50% output



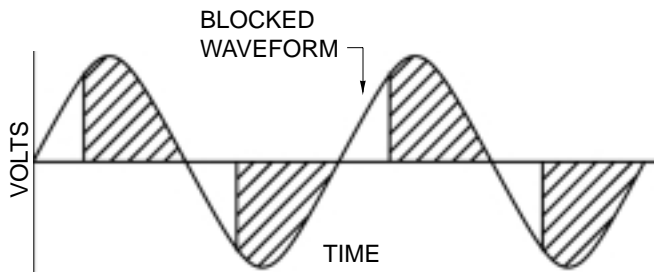
at 75% demand the time base would be 1/15 of a second or four cycles, etc.

FIGURE 3 - Variable time base at 75% output



Zero crossover firing is used to control resistive loads which change little with aging and temperature. Since the voltage is switched at zero amplitude, negligible radio frequency interference (RFI) is generated.

ii) A second method of gate switching is **phase angle firing** where a part of each waveform is blocked.



Phase angle firing is most frequently used on inductive loads with high inrush currents. If possible, it is best to avoid phase angle type SCR's since RFI may be generated.

Fortunately, with Caloritech™ equipment we seldom have to resort to this type of control.

ADVANTAGES

SCR switching has as its main advantage the ability to switch loads at high speed. Properly employed, they can contribute to excellent system temperature control and prolong heater service life.

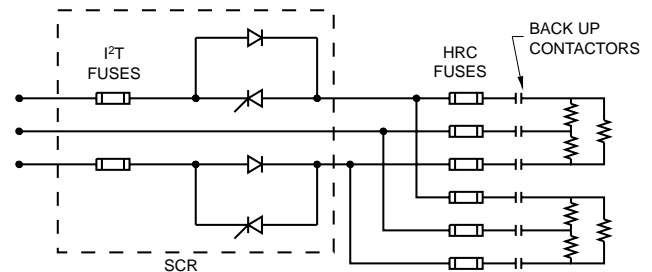
They are silent during operation and, if sized conservatively, will prove to be low maintenance devices.

PROTECTION

SCR's can fail "ON" and it is vital to protect the device against short circuits at the load. Special I²t semiconductor fuses are utilized for this purpose. Back-up fused magnetic contactors are frequently employed as in Figure 4. These contactors can be de-energized by a limit device but in the normal state they remain closed allowing the full load to be switched by the SCR.

With contactors, it is most economical to limit switching to 45 amps, and for this reason the load is usually divided into smaller circuits.

FIGURE 4 - SCR with back-up contactors



FIRING BOARDS

Packaged SCR's incorporate a firing board which is essentially an electronic circuit that accepts various inputs from a temperature controller and converts these inputs into a corresponding gate signal.

HEAT SINKS

All solid state switches have an internal resistance which is converted into heat when the SCR is in the conduction mode. High surface area aluminum heat sinks are used to transfer this heat away from the silicon wafer. For larger SCR's, cooling fans are also required for this purpose.

SCR - AS A PACKAGED CONTROL

As a matter of convenience, current practice is to call the combination of component SCR's, firing board, heat sink, fusing, fan, enclosure, interconnecting wiring, etc. an SCR! It's probably best to adopt this "control" meaning as opposed to the more limited (but more correct) "component" meaning.

A. Power Requirement for Initial Heat-up

1. Heat absorbed by all materials:

$$\frac{\text{Weight of material (lb)} \times \text{Specific heat (Btu/lb-°F)} \times \text{Temperature difference (final - initial) (°F)}}{3412(\text{Btu/kWh})} = \text{_____ kWh}$$

Note: The above step must be repeated for each material heated. See Tables 1, 2, 3, and 4 on pages D38 and D39 for specific heats and weights.

2. Heat required for fusion or vaporization:

$$\frac{\text{Weight of material (lb)} \times \text{Heat of fusion or vaporization (Btu/lb)}}{3412 (\text{Btu/kWh})} = \text{_____ kWh}$$

Note: When the specific heat of a material changes at some temperature during the heat-up, due to melting (fusion) or evaporation (vaporization), perform Step 1 for the heat absorbed from the initial temperature up to the temperature at the point of change, add Step 2, then repeat Step 1 for heat absorbed from the point of change to the final operation temperature. See Tables 1, 2, 3, and 4 on pages D38 and D39 for heats of fusion and vaporization and temperatures at which these changes in state occur.

3. Heat required to replace average heat losses:

$$\frac{\text{Exposed surface area (sq. ft.)} \times \text{Heat loss at final operating temperature (W/sq. ft.)} \times \text{Time allowed for heat-up (hrs)}}{1000 (\text{W/kW})} \times \frac{1}{2} \left(\begin{array}{l} \text{to obtain an} \\ \text{average loss} \end{array} \right) = \text{_____ kWh}$$

Note: See Figures 1 - 4 on pages D40 and D41 for normal heat losses

$$\text{4. Heat to provide for contingencies, Safety Factor: } 20\% [\text{Step 1 (kWh)} + \text{Step 2 (kWh)} + \text{Step 3 (kWh)}] = \text{_____ kWh}$$

$$\text{Total Heat Requirement for Initial Heat-up:} = \text{_____ kWh}$$

$$\text{Total Power Requirement for Initial Heat-up:} \frac{\text{Step 1 (kWh)} + \text{Step 2 (kWh)} + \text{Step 3 (kWh)} + \text{Step 4 (kWh)}}{\text{Time allowed for heat-up (hrs)}} = \text{_____ kW}$$

B. Power Requirement for Operating Heat

1. Heat absorbed by all materials added to the process:

$$\frac{\text{Weight of material added (lb)} \times \text{Specific heat (Btu/lb-°F)} \times \text{Temperature difference (final - initial) (°F)}}{3412(\text{Btu/kWh})} = \text{_____ kWh}$$

Note: The above step must be repeated for each material heated. See Tables 1, 2, 3, and 4 on pages D38 and D39 for specific heats and weights.

2. Heat required for fusion or vaporization during process:

$$\frac{\text{Weight of material (lb)} \times \text{Heat of fusion or vaporization (Btu/lb)}}{3412 (\text{Btu/kWh})} = \text{_____ kWh}$$

Note: When the specific heat of a material changes at some temperature during the heat-up, due to melting (fusion) or evaporation (vaporization), perform Step 1 for the heat absorbed from the initial temperature up to the temperature at the point of change, add Step 2, then repeat Step 1 for heat absorbed from the point of change to the final operation temperature. See Tables 1, 2, 3, and 4 on pages D38 and D39 for heats of fusion and vaporization and temperatures at which these changes in state occur.

3. Heat required to replace heat losses:

$$\frac{\text{Exposed surface area (sq. ft.)} \times \text{Heat loss at final operating temperature (W/sq. ft.)} \times \text{Working cycle time (hrs)}}{1000 (\text{W/kW})} = \text{_____ kWh}$$

Note: See Figures 1 - 4 on pages D40 and D41 for normal heat losses

$$\text{4. Heat to provide for contingencies, Safety Factor: } 20\% [\text{Step 1 (kWh)} + \text{Step 2 (kWh)} + \text{Step 3 (kWh)}] = \text{_____ kWh}$$

$$\text{Total Heat Requirement per Working Cycle:} = \text{_____ kWh}$$

$$\text{Total Power Requirement for Operating Heat:} \frac{\text{Step 1 (kWh)} + \text{Step 2 (kWh)} + \text{Step 3 (kWh)} + \text{Step 4 (kWh)}}{\text{Working cycle time (hrs)}} = \text{_____ kW}$$

Heating Liquids (Water)

An open steel tank, 2 ft. wide, 3 ft. long, 2 ft. deep and weighing 270 lbs., is filled with water to within 6 inches of the top. Bottom and sides have 3 inches of insulation. Water is to be heated from 50°F to 150°F within 2 hours and, from then on, approximately 4 gallons per hour will be drawn off and replaced.

From Table 1 on page D38, Specific Heat of steel:
0.12 Btu/lb.-°F

From Table 3 on page D39, Specific Heat of water:
1.0 Btu/lb.-°F

From Table 3 on page D39, Weight of water:
62.5 lb./cu. ft. (8.3 lb./gal.)

Water in tank:
(2 x 3 x 1.5)cu. ft. x 62.5 lb./cu. ft. = 563 lb.

From Fig. 3 on page D41, Water surface loss at 150°F:
270 W/sq. ft.

From Fig. 4 on page D41, Insulated wall loss at 100°F rise:
7 W/sq. ft.

A. INITIAL HEAT-UP REQUIREMENT

- 1a.** To heat water:
$$\frac{563 \text{ lb.} \times 1.0 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 50)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 16.5 \text{ kWh}$$
- 1b.** To heat tank:
$$\frac{270 \text{ lb.} \times 0.12 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 50)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.95 \text{ kWh}$$
- 2.** Heat of fusion or vaporization: None
- 3a.** Average water surface loss:
$$\frac{6 \text{ sq. ft.} \times 270 \text{ W/sq. ft.} \times 2 \text{ hrs.}}{1000 \text{ W/kWh} \times 2} = 1.62 \text{ kWh}$$
- 3b.** Average tank surface loss:
$$\frac{26 \text{ sq. ft.} \times 7 \text{ W/sq. ft.} \times 2 \text{ hrs.}}{1000 \text{ W/kWh} \times 2} = 0.18 \text{ kWh}$$
- 4.** Safety factor:
20% (16.5 + 0.95 + 1.62 + 0.18) = 3.85 kWh
- Total Heat Requirement** = 23.10 kWh
- Power Required for Initial Heat-up:**
23.10 kWh / 2 hrs. = 11.55 kW

B. OPERATING REQUIREMENT

- 1.** To heat additional water
$$\frac{4 \text{ gal./hr.} \times 8.3 \text{ lb./gal.} \times 1.0 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 50)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.97 \text{ kW}$$
- 2.** Heat of fusion or vaporization: None
- 3a.** Water surface loss:
$$\frac{6 \text{ sq. ft.} \times 270 \text{ W/sq. ft.}}{1000 \text{ W/kWh}} = 1.62 \text{ kW}$$
- 3b.** Tank surface loss:
$$\frac{26 \text{ sq. ft.} \times 7 \text{ W/sq. ft.}}{1000 \text{ W/kWh}} = 0.18 \text{ kW}$$
- 4.** Safety factor:
20% (0.97 + 1.62 + 0.18) kW = 0.55 kW
- Power Required for Operation** = 3.32 kW

Melting Solids (Paraffin)

An open top uninsulated steel tank, 1½ ft. wide, 2 ft. long, 1½ ft. deep, and weighing 140 lb., contains 168 lb. of paraffin to be heated from 70°F to 150°F in 2 hours. Steel drills, each weighing 0.157 lb. are to be placed in a 60 lb. rack and dip coated in the melted paraffin. 1500 drills can be processed per hour with 20 lb. of paraffin.

From Table 1 pg. D38, Specific Heat of steel: 0.12 Btu/lb.-°F
From Table 2 pg. D38, Specific Heat of solid paraffin: 0.70 Btu/lb.-°F

From Table 2 pg. D38, Melting Point of paraffin: 133°F
From Table 2 pg. D38, Heat of Fusion of paraffin: 63 Btu/lb.
From Table 3 pg. D39, Specific Heat of melted paraffin: 0.71 Btu/lb.-°F

From Fig. 3 pg. D41, Paraffin surface loss at 150°F: 70 W/ft.²

From Figs. 1 & 2 pg. D40, Steel surf. loss at 150°F: 55 W/ft.²

A. INITIAL HEAT-UP REQUIREMENT

- 1a.** To heat tank:
$$\frac{140 \text{ lb.} \times 0.12 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 70)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.39 \text{ kWh}$$
- 1b.** To heat solid paraffin:
$$\frac{168 \text{ lb.} \times 0.70 \text{ Btu/lb.-}^\circ\text{F} \times (133 - 70)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 2.17 \text{ kWh}$$
- Fusion occurs at this point**
- 1c.** To heat melted paraffin:
$$\frac{168 \text{ lb.} \times 0.71 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 133)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.59 \text{ kWh}$$
- 2.** Heat of fusion, to melt paraffin
$$\frac{168 \text{ lb.} \times 63 \text{ Btu/lb.}}{3412 \text{ Btu/kWh}} = 3.10 \text{ kWh}$$
- 3a.** Average paraffin surface loss:
$$\frac{3 \text{ sq. ft.} \times 70 \text{ W/sq. ft.} \times 2 \text{ hrs.}}{1000 \text{ W/kWh} \times 2} = 0.21 \text{ kWh}$$
- 3b.** Average tank surface loss:
$$\frac{13.5 \text{ sq. ft.} \times 55 \text{ W/sq. ft.} \times 2 \text{ hrs.}}{1000 \text{ W/kWh} \times 2} = 0.74 \text{ kWh}$$
- 4.** Safety factor:
20% (0.39 + 2.17 + 0.59 + 3.10 + 0.21 + 0.74) = 1.44 kWh
- Total Heat Requirement** = 8.64 kWh
- Power Required for Initial Heat-up:**
8.64 kWh / 2 hrs. = 4.32 kW

B. OPERATING REQUIREMENT

- 1a.** To heat drills and rack:
$$\frac{(1500 \times 0.157 + 60) \text{ lb./hr.} \times 0.12 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 70)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.83 \text{ kW}$$
- 1b.** To heat additional solid paraffin:
$$\frac{20 \text{ lb./hr.} \times 0.70 \text{ Btu/lb.-}^\circ\text{F} \times (133 - 70)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.26 \text{ kW}$$
- Fusion occurs at this point**
- 1c.** To heat additional melted paraffin:
$$\frac{20 \text{ lb./hr.} \times 0.71 \text{ Btu/lb.-}^\circ\text{F} \times (150 - 133)^\circ\text{F}}{3412 \text{ Btu/kWh}} = 0.07 \text{ kW}$$
- 2.** Heat of fusion, to melt additional paraffin:
$$\frac{20 \text{ lb./hr.} \times 63 \text{ Btu/lb.}}{3412 \text{ Btu/kWh}} = 0.37 \text{ kW}$$
- 3a.** Paraffin surface loss:
$$\frac{3 \text{ sq. ft.} \times 70 \text{ W/sq. ft.}}{1000 \text{ W/kWh}} = 0.21 \text{ kW}$$
- 3b.** Tank surface loss:
$$\frac{13.5 \text{ sq. ft.} \times 55 \text{ W/sq. ft.}}{1000 \text{ W/kWh}} = 0.74 \text{ kW}$$
- 4.** Safety factor:
20% (0.83 + 0.26 + 0.07 + 0.37 + 0.21 + 0.74) kW = 0.50 kW
- Power Required for Operation** = 2.98 kW

TABLE 1 - PROPERTIES OF METALS

Material	Average specific heat Btu/(lb.)(°F)	Latent heat of fusion Btu/lb.	Density lbs./in. ³	Melting point °F (lowest)	Thermal Conductivity K	Thermal expansion in./in.°F x10 ⁻⁶
					(Btu)(in.) (hr.)(sq.ft.)(°F)	
Aluminum	.24	169	.098	1190	1540	13.1
Antimony	.049	69	.239	1166	131	
Babbit - lead base	.039		.370	470	165.6	
Babbit - tin base	.071		.267	465	278.4	
Barium	.068		.130	1562		
Beryllium	.052		.066	2345	1121.0	
Bismuth	.031	22.4	.353	520	59	
Boron	.309		.083	4172		
Brass (80-20)	.091		.310	1700	82	
Brass (70-30)	.10		.304	1700	672	
Brass (yellow)	.096		.306	1710	830	11.2
Bronze (75/25)	.082		.313	1832	180	
Cadmium	.055	75	.313	610	660	
Calcium	.149	140	.056	1564	912	
Carbon	.165		.080	6422	173	
Chromium	.11		.260	2822	484	
Cobalt	.099	115.2	.321	2696	499	
Constantan	.098		.321			
Copper	.095	91.1	.322	1981	2680	9.8
German silver	.109		.311	1761	168	
Gold	.032	29.0	.698	1945	2030	7.9
Incoloy 800	.13		.290	2500	80	7.9
Incoloy 600	.126		.304	2500	103	5.8
Inconel 600	.11		.304	2470	109	5.8
Iron, cast	.12		.260	2150	346	6.0
Iron, wrought	.12		.278	2800	432	
Lead, solid	.032	11.3	.410	620	240	16.4
Lead, liquid	.037		.387		108	
Linotype	.04		.363	480		
Lithium	.79	59	.212	367	516	
Magnesium	.27	160	.063	1202	1106	14
Manganese	.115	116	.268	2268	80.6	
Mercury	.033	5.0	.488	-38	60.8	
Molybdenum	.071	126	.369	4750	980	2.94
Monel 400	.11		.319	2400	151	6.4
Nickel 200	.12	133	.321	2615	520	5.8
Nichrome	.11		.302	2550	104	7.3
Platinum	.035	49	.775	3225	480	4.9
Potassium	.058	26.2	.434	146	720	
Rhodium	.059		.449	3570	636	
Silicon	.162		.008	2570	600	
Silver	.057	38	.379	1760	2900	10.8
Sodium	.295	49.5	.035	207	972	
Solder	.051	17	.323	361	310	13.1
Steel, mild	.122		.284	2760	460	6.7
Stn. Stl. 304	.12		.286	2550	105	9.6
Stn. Stl. 430	.11		.275	2650	155	6.0
Tantalum	.035		.60	5425	375	3.57
Tin, liquid	.052		.253		218	
Tin, solid	.065	26.1	.263	450	455	13
Titanium	.13		.164	3035	112	4.7
99.0 % Tungsten	.040	79	.697	6170	1130	2.45
Type Metal	.040	14	.388	500	180	
Uranium	.028		.677	3075	193.2	
Zinc	.096	43.3	.258	787	740	22.1
Zirconium	.067	108	.234	3350	145	3.22

TABLE 2 - PROPERTIES OF NON-METALLIC SOLIDS

Material	Average specific heat Btu/(lb.)(°F)	Latent heat of fusion Btu/lb.	Average Density lbs./in. ³	Melting point °F (lowest)	Thermal Conductivity K	Thermal expansion in./in.°F x10 ⁻⁶
					(Btu)(in.) (hr.)(sq.ft.)(°F)	
ABS Plastic	.35		.042		1.32	
Acrylic	.34		.041		2.28	
Alumina			.087		1.0	
Aluminum Silicate	.2		.086	3690	9.1	
Asbestos	.25		.021		.44	
Ashes	.2		.025		.49	
Asphalt	.40		.046		5.3	
Bakeligh, Pure Resin	.3 - .4		.045			
Barium Chloride	.10		.139	1697		
Beeswax		75	.035	144	1.67	
Boron Nitride	.33		.082	5430	125	1 - 4

TABLE 2 - PROPERTIES OF NON-METALLIC SOLIDS (cont)

Material	Average specific heat Btu/(lb.)(°F)	Latent heat of fusion Btu/lb.	Average Density lbs./in. ³	Melting point °F (lowest)	Thermal Conductivity K	Thermal expansion in./in.°F x10 ⁻⁶
					(Btu)(in.) (hr.)(sq.ft.)(°F)	
Brickwork	.22		.076		3 - 7	3 - 6
Calcium Chloride	.17	72	.091	1422		
Carbon	.28		.080	6700	165	0.3 - 2.4
Canaba Wax	.8		.036			
Cellulose						
Acetate	.3 - .5		.047		1.2 - 2.3	61 - 83
Cement	.19		.054		2.04	
Ceramic Fiber	.27		.007			
Chalk	.215		.083		5.76	
Clay	.224		.052	3160	9	
Coal (Coarse Anthracite)	.32		.046		11	
Coal Tars	.35 - .45		.045			
Coke	.265		.043			
Concrete (Cinder)	.16		.058		5.3	
Concrete (Stone)	.156		.083		9.5	
Cork	.5		.008		.36	
Cotton (Flax, Hemp)	.31		.053		.41	
Delrin	.35		.051		1.6	45
Diamond	.147		.127		13872	
Earth, Dry & Packed	.44		.054		.9	
Epoxy	.25 - .3		.045		1.2 - 2.4	
Ethyl Cellulose	.32 - .46		.041			
Fiberglass			.0004		.28	
Firebrick, Fireclay	.243		.083	2900	6.6	
Firebrick, Silica	.258		.089	3000	7.2	
Flourspar	.21		.081		1.68	
Fluoroplastics	.28		.101		7.5	5
Glass, crown	.161		.097		13 - 28	
Granite	.192		.075		1.25	
Graphite	.20					
Ice	.53	144	.0324	32	1.1	28.3
Isoprene	.48		.034		10	
Limestone	.217		.088		3.6-9	
Magnesia	.234		.130	5070	.48	
Magnesite						
Brick	.222		.092		10.8 - 30	
Magnesium Silicate			.101		15.6	
Marble	.21		.097		14.4	
Marinite I @ 400°F	.29		.027		.89	
Mica	.21		.102		3.0	18
MgO (Before Compacted)	.21		.085		3.6	
MgO (Compacted)	.209		.112		20	7.7
Nylon	.4		.040		1.5	61 - 63
Paper	.45		.034		.82	
Paraffin	.70	63	.032	133	1.6	
Phenolic Plastic	.35		.060		1.02	
Phenolic Resin, Cast	.3 - .4		.049		1.1	
Phenolic, Sheet or Tube Laminated Pitch, Hard	.3 - .5		.045	300	2.4	
Polycarbonate	.3		.044		1.38	
Polyester	.2 - .35		.046		3.96 - 5	
Polyethylene	.55		.035		2.3	94
Polypropylene	.46		.032		1.72	
Polystyrene	.32		.038		.7 - 1.0	33 - 44
Polyvinyl Chloride						
Acetate	.2 - .3		.049		.84 - 1.2	
Porcelain	.26		.087		6 - 10	
Potassium Chloride	.17		.072	1454		
Potassium Nitrate	.26		.076	633		
Quartz	.26		.080		9.6	
Rock Salt	.219		.044	1495		
Rubber	.44				1.1	340

TABLE 2 - PROPERTIES OF NON-METALLIC SOLIDS (cont)

Material	Average specific heat Btu/(lb.)(°F)	Latent heat of fusion Btu/lb.	Average Density lbs./in. ³	Melting point °F (lowest)	Thermal Conductivity K $\frac{(Btu)(in.)}{(hr)(sq.ft.)(°F)}$	Thermal expansion in./in.°F x10 ⁻⁶
Sand, Dry	.191		.054		2.26	
Sandstone	.22		.081			
Silica (fused)	.316				10.0	
Silicon Carbide	.20 - .23		.069		105	
Silicone Rubber	.45		.045		1.5	
Soapstone	.22		.097		11.3	
Sodium Carbonate	.30		.078	520		
Sodium Chloride	.22		.078	1474		
Sodium Cyanide	.30		.054	1047		
Sodium Nitrate	.29		.082	584		
Sodium Nitrite	.30		.078	520		
Soil, Dry						
Steatite	.20		.094		17.5 - 23	4.5 - 5.5
Stone	.20					
Sugar	.30		.061	320		
Sulfur	.175	17	.075	246	1.9	36
Tallow			.035	90		
Teflon	.25		.078		1.7	55
Urea, Formaldehyde	.4		.056		.8 - 2.0	28 - 100
Vinyl	.3 - .5		.046			
Wood, Oak	.57		.029			

TABLE 3 - PROPERTIES OF LIQUIDS

Material	Average specific heat Btu/(lb.)(°F)	Heat of vaporization Btu/lb.	Density lbs./U.S. Gal.	Boiling point °F	Thermal Conductivity K $\frac{(Btu)(in.)}{(hr)(sq.ft.)(°F)}$
Acetic acid, 20%	.91	810	8.6	214	3.7
Acetic acid, 100%	.48	175	8.7	245	1.14
Acetone, 100%	.514	225	6.5	133	1.15
Alcohol (allyl)	.665	293	7.4	207	
Alcohol (amyl)	.65	216	7.4	280	
Alcohol (butyl)	.687	254	6.1	244	
Alcohol (ethyl)	.60	367	6.6	173	1.3
Alcohol (propyl)	.57	295.2	6.7	208	
Ammonia, 100%	1.1	589	6.4	-27	3.48
Asphalt	.42		8.3		5.04
Benzene	.42	170	7.5	175	1.04
Brine (25% CaCl)	.689		10.2		3.36
Brine (25% NaCl)	.786	730	9.9	220	2.88
Brine (25% NiCl)	.81	728	9.9	221	4.0
Carbon Tetrachloride	.21		13.2	170	
Caustic soda (18%)	.84	795	10.0	221	3.9
Corn Syrup					
Dextrose	.65		11.7	231	
Cottonseed Oil	.47		7.9		1.2
Dowtherm A	.44	42.2	8.8	496	.96
Ether	.503	160	6.1	95	.95
Ethyl Acetate	.475	183.5	6.9	180	
Ethyl Bromide	.215	108	12.1	101	
Ethyl Chloride	.367	166.5	7.6	54	
Ethyl Iodide	.161	81.3	15.1	160	
Ethylene Bromide	.172	83	16.0	270	
Ethylene Chloride	.299	139	9.6	240	
Ethylene Glycol	.555		9.4	387	
Formic Acid	.525	216	9.3	213	
Freon 11	.208		12.3	74.9	.600
Freon 12	.232	62	10.9	-21.6	.492
Freon 22	.300		10.0	-41.36	.624
Fuel Oil #1	.47	86	6.8	440	1.008
Fuel Oil #2	.44		7.2		.96
Fuel Oil #3, #4	.425	67	7.4	580	.918
Fuel Oil #5, #6	.41		7.9		.852
Gasoline	.53	116	5.5 - 5.7	280	.936
Glycerine	.61		10.5	556	2.0
Heptane	.49	137.1	5.1	210	
Hexane	.6	142.5	5.1	155	
Hydrochloric 10%	.93		8.9	221	3.9
Ice	.5		7.5		3.96
Lard	.64		7.7		
Linseed Oil	.44		7.7	552	
Mercury	.033	117	113.0	675	59.64
Methyl Acetate	.47	176.5	7.3	133	
Methyl Chloroform	.26	95	11.1	165	

TABLE 3 - PROPERTIES OF LIQUIDS (continued)

Material	Average specific heat, Btu/(lb.)(°F)	Heat of vaporization Btu/lb.	Density lbs./U.S. Gal.	Boiling point °F	Thermal Conductivity K $\frac{(Btu)(in.)}{(hr)(sq.ft.)(°F)}$
Methylene Chloride	.288	142	11.0	104	
Molasses	.60		11.7	220	
NaK (78% K)	.21		6.2	1446	167.0
Napthalene	.396	103	7.2	424	
Nitric acid, 7%	.92	918	8.6	220	3.8
Nitric acid, 95%	.5	207	12.5	187	
Nitrobenzene	.35	142.2		412	
Oil (SAE10-30)	.43		7.4		
Oil (SAE40-50)	.43		7.4		
Olive Oil	.47		7.8	570	
Paraffin (melted)	.71		6.3		1.0
Perchloroethylene	.21	90	13.5	250	
Phenol	.56		8.9	346	
Phosphoric 10%	.93		8.7		
Phosphoric 20%	.85		9.2		
Potassium (K)	.18	893	6.0	1400	320.0
Propane (Comp)	.576		0.02	-48.1	1.81
Sea Water	.94		8.6		
Sodium (Na)	.30	1810	6.8	1621	580.0
Sodium Hydroxide 30% Solution	.84		11.1		
50% Solution	.78		12.8		
Soybean Oil	.24-.33		7.7		
Starch			12.8		
Sucrose, 40% Sugar	.66		9.8	214	
Sucrose, 60% Sugar	.74		10.7	218	
Sulfur, Melted 500°F	.24	120	15.0	832	
Sulfuric acid, 10%	.92		9.9	216	4.0
Sulfuric acid, 20%	.84		9.5	218	
Sulfuric acid, 60%	.52	219	12.5	282	2.88
Sulfuric acid, 98%	.35		15.3	625	1.8
Therminol FR-2	.30		12.1	648	.70
Toluene	.42		7.2		1.032
Trichloroethylene	.23	103	12.2	188	.84
Transformer Oils	.42		7.5		.9
Turpentine	.41	123	7.3	318	.90
Vegetable oil	.43		7.7		1.1
Water	1.0	970	8.3	212	4.2
Xylene	.411	149.2	7.2	288	

TABLE 4 - PROPERTIES OF GASES

Gas	Specific heat Btu/lb.°F	Density lbs./ft. ³	Thermal Conductivity K $\frac{(Btu)(in.)}{(hr)(sq.ft.)(°F)}$
Acetylene	.35	.073	.129
Air at 80°F	.240	.073	.18
at 400°F	.245	.046	.27
Alcohol, Ethyl (Vapor)	.4534		
Alcohol, Methyl (Vapor)	.4580		
Ammonia	.523	.044	.16
Argon	.125	.102	.12
Butane		.1623	.0876
Butylene		.148	
Carbon dioxide	.199	.113	.12
Carbon monoxide	.248	.072	.18
Chlorine	.115	.184	.06
Chloroform	.1441		.046
Chloromethane	.24	.1309	.0636
Ethyl Chloride	.1703		.066
Ethyl Ether	.4380		.0924
Ethylene	.40	.0728	.1212
Helium	1.25	.011	1.10
Hydrochloric Acid	.191	.0946	
Hydrogen	3.39	.0052	.13
Hydrogen Sulfide	.2451	.096	.091
Methane	.528	.041	.25
Nitric Oxide	.231	.0779	.1656
Nitrogen	.248	.072	.19
Nitrous Oxide	.221	.1143	1.056
Oxygen	.218	.082	.18
Sulphur dioxide	.152	.172	.07
Water Vapor (212°F)	.482	.0372	.16

TABLE 1 - PROPERTIES OF AIR

Temp. (°F)	Specific Heat (BTU/lb.°F)	Density (lb./ft. ³)
0	.240	.086
50	.240	.078
100	.240	.071
150	.241	.065
200	.242	.060
250	.243	.056
300	.244	.052
350	.245	.049
400	.247	.046
500	.249	.041
600	.252	.037
700	.254	.034
800	.257	.032
900	.260	.029
1000	.262	.027
1100	.265	.025
1200	.267	.024

TABLE 2 - THERMAL CONDUCTIVITY OF INDUSTRIAL INSULATION

Type of Insulation	Maximum Service Temp. (°F)	Typical K Values BTU/hr./sq.ft./°F/in.					
		Mean Temp. (°F) Between Inner and Outer Insulation Surface					
		100	200	300	500	700	900
Mineral Wool Blanket flexible felt	450	.26	.34	.45			
Mineral Wool Block and Board resin binder	600	.28	.35	.43			
85% Magnesia Block and Board	600	.35	.38	.42	.46		
Foam Glass Block and Board	800	.41	.48	.55			
Calcium Silicate low density	1200	.38	.41	.44	.52	.62	.72
Mineral Wool Blanket metal reinforced	1200	.29	.35	.42	.56		
Silica Lime Block and Board	1200	.33	.38	.43	.53	.64	.75
Mineral Wool Block and Board inorganic binder	1600	.34	.39	.44	.54	.64	
Calcium Silicate high density	1800				.63	.74	.95

TABLE 3 - VISCOSITIES

Material	SSU			CENTIPOISE		
	4.4°C	26.7°C	49°C	4.4°C	26.7°C	49°C
	40°F	80°F	120°F	40°F	80°F	120°F
Asphalt RS-1 MS-1 SS-1	400	160			86	34
Asphalt RC-0 MC-0 SC-0	950	340				
Asphalt RC-3 MC-3 SC-3	40000	7000				
Asphalt RC-5 MC-5 SC-5	500000	45000				
Asphalt 100-120 penetration	3500 at 250°F					
Asphalt 40-50 penetration	8000 at 250°F					
Benzene				.8	.62	.46
Gasoline				.7	.55	.44
No.1 Fuel Oil (Kerosene)	40	36		3.3	2.1	1.4
No.2 Fuel Oil - PS100	43	36	33	4.6	2.6	1.6
No.3 Fuel Oil - PS200	84	52	41	15.0	7.0	4.0
No.4 Fuel Oil	480	125	62	92.0	24.0	9.6
No.5 Fuel Oil - PS300		1600	370		390.0	75.0
No.6 Fuel Oil, Bunker C		4500	650		1000.0	155.0
Transformer Oil, Light	170	72	49	34.2	12.1	6.3
Transformer Oil, Medium	460	145	70	89.0	28.2	11.9
34°API Mid-continent crude	88	51	37	15	6.5	3.0
28°API gas oil	135	59	48	25	9.0	6.0
Quench and tempering Oil						
SAE-5W	550	160	74			
SAE-10W	1500	265	120	170	50	22
SAE-20	2900	500	170			
SAE-30	5000	870	260	1200	200	60
SAE-40	8500	1400	380			
SAE-50	23000	3600	720	400	100	

Figure 1 - Heat losses from uninsulated smooth solid surfaces (60 - 180°F). Assumed external ambient temperature of 70°F.

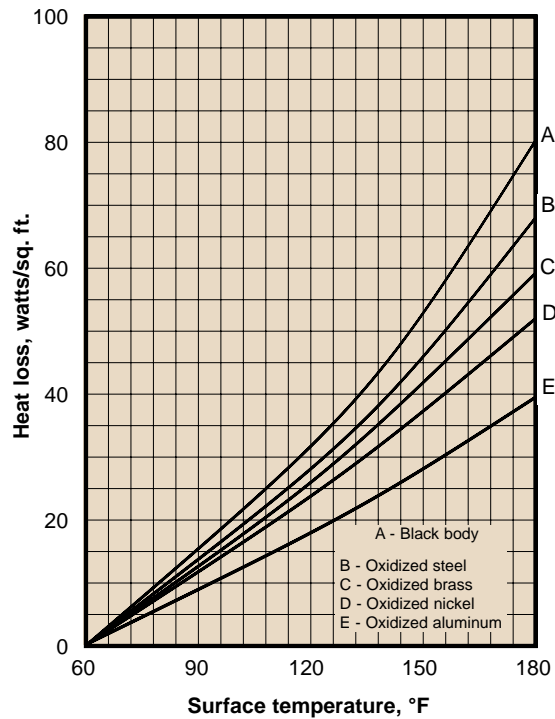


Figure 2 - Heat losses from uninsulated smooth solid surfaces (150 - 1000°F). Assumed external ambient temperature of 70°F.

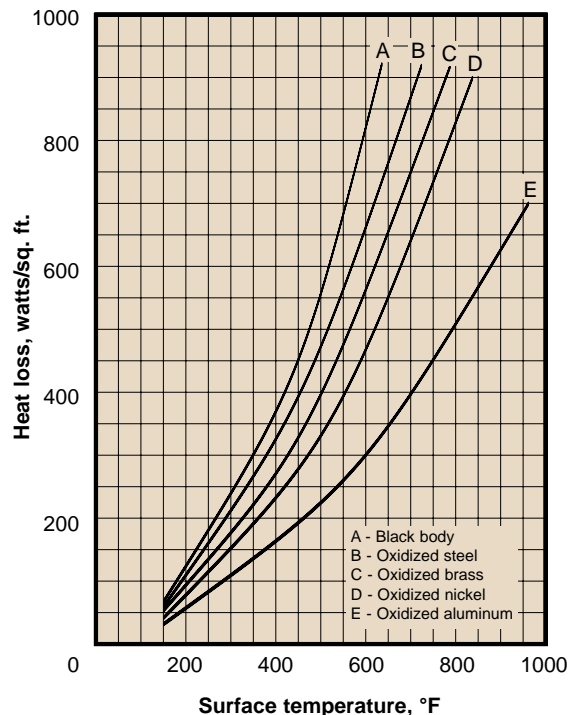


Figure 3 - Heat losses from liquid surfaces. Assumed external ambient temperature of 70°F.

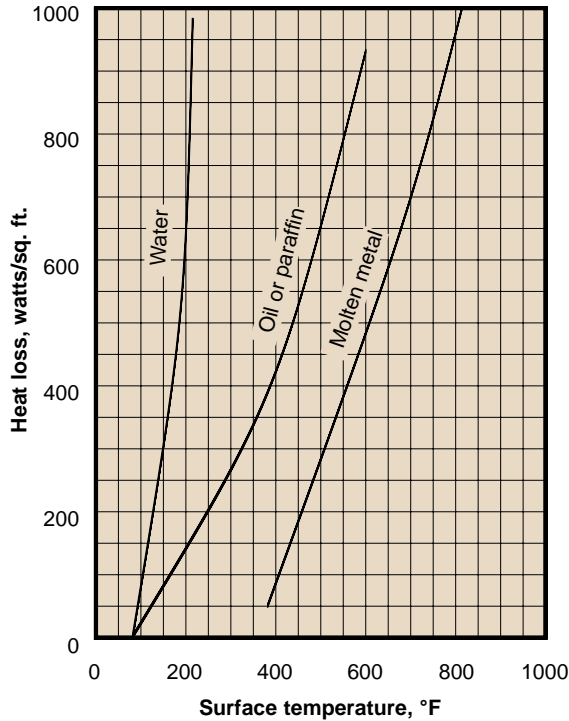
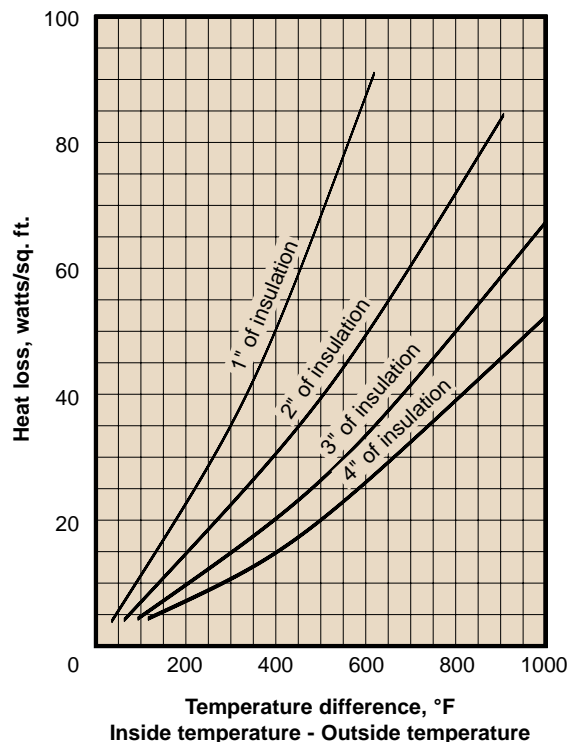


Figure 4 - Heat losses from insulated walls. Curves are for standard high-grade material, such as 85% magnesia, Rockwool, etc.



WIND VELOCITY AND HEAT LOSS

Wind velocity will increase surface heat losses. Table 1 can be used as a guide for estimating the factors to be applied to the still air heat losses from Figs. 1, 2 and 4.

TABLE 1 - WIND VELOCITY FACTORS

WIND VELOCITY (MPH)	WELL SEALED INSULATED SURFACE			UNINSULATED SURFACE (TEMP. °F)		
	1"	2"	3"	200	600	1000
5	-	-	-	1.7	1.5	1.3
10	-	-	-	2.1	1.7	1.4
15	1.1	-	-	2.4	2.0	1.6
20	1.2	1.1	-	2.7	2.3	1.7
25	1.3	1.2	1.1	3.0	2.6	1.8
30	1.4	1.3	1.2	3.3	3.0	1.9

HEAT LOSSES FROM INSULATED PIPES

To find the heat loss from the insulated pipes, in watts/ft. multiply the appropriate factor from Table 2 by the °F difference between the pipe holding temperature and the minimum ambient temperature.

If the pipe holding temperature is above 200°F, multiply the above answer by 1.2.

TABLE 2 - HEAT LOSS FACTORS FOR PIPE

PIPE SIZE	INSULATION THICKNESS AND FACTORS						
	1/2"	1"	1 1/2"	2"	2 1/2"	3"	4"
1/2	0.086	0.054	0.043	0.037			
1/4	0.102	0.062	0.048	0.041			
1	0.123	0.073	0.056	0.047			
1 1/4	0.142	0.083	0.063	0.052			
1 1/2	0.164	0.094	0.070	0.058			
2	0.192	0.109	0.081	0.066			
2 1/2	0.229	0.128	0.093	0.076			
3	0.259	0.142	0.107	0.083			
3 1/2	0.287	0.157	0.113	0.091			
4	0.316	0.172	0.123	0.098	0.083	0.073	0.060
4 1/2	0.347	0.189	0.134	0.107	0.090	0.079	0.065
5	0.417	0.219	0.155	0.121	0.103	0.089	0.073
6	0.472	0.250	0.174	0.136	0.114	0.099	0.080
7	0.526	0.275	0.192	0.151	0.126	0.109	0.088
8	0.571	0.305	0.212	0.166	0.137	0.119	0.095
9	0.634	0.338	0.234	0.183	0.151	0.130	0.104
10	0.634	0.338	0.234	0.183	0.151	0.130	0.104
12	0.776	0.397	0.275	0.212	0.175	0.149	0.119
14	0.834	0.431	0.298	0.230	0.190	0.162	0.128
16	0.961	0.498	0.334	0.258	0.212	0.181	0.142
18	1.088	0.555	0.379	0.289	0.236	0.200	0.156
20	1.190	0.598	0.416	0.319	0.260	0.219	0.171
24	1.430	0.731	0.490	0.374	0.305	0.259	0.200

Galvanic Corrosion

Table 1 is the galvanic series of commonly used metals when immersed in sea water. This list will vary slightly when a different electrolyte forms the galvanic couple.

Metals which are grouped show negligible corrosion when joined.

For galvanic corrosion to occur the following conditions must be met.

- i) Two or more electrochemically dissimilar metals are present and in electrical contact (which is not necessarily physical contact).
- ii) The metals must be in contact with an electrolyte.

Quite often other types of corrosion are incorrectly attributed to galvanic corrosion. If the foregoing conditions are met and the corrosion is localized near the junction of the metals, it was probably caused by galvanic effects. Otherwise, look elsewhere.

The best one can do is to try to avoid designs which involve electrically coupled metals. This is not always practical. However, the choice of metals can help to lessen corrosive effects. Try to select metals as close together as possible on the galvanic series.

Keep in mind that the least noble or more active metal will deplete during corrosion. Never couple a small anode with a large cathode.

Quite often it is practical to electrically insulate the metals from one another. If it is determined that dissimilar uninsulated metals must be used, make the anodic part of heavier material. Also, design the part for easy replacement.

Useful Corrosion Terminology

BIMETALLIC CORROSION - Galvanic corrosion.

CORROSION-EROSION - Corrosion which is increased because of the abrasive action of a moving stream.

CREVICE CORROSION - Localized corrosion resulting from the formation of a concentration cell in a crevice formed between a metal and a nonmetal or between two metal surfaces.

FRETTING CORROSION - Fretting refers to metal deterioration caused by repetitive slip at the interface between two surfaces.

HYDROGEN EMBRITTLEMENT - Embrittlement of a metal caused by hydrogen.

IMPINGEMENT ATTACK - Erosion-corrosion caused by turbulence or impinging flow at certain points.

INTERGRANULAR CORROSION - Corrosion which occurs preferentially at grain boundaries.

PITTING - Highly localized corrosion resulting in deep penetration at only a few spots.

SCALING - High temperature corrosion resulting in formation of thick corrosion product layers.

STRESS CORROSION - Corrosion which is accelerated by stress.

TABLE 1 - GALVANIC SERIES OF COMMONLY USED METALS WHEN EXPOSED TO SEA WATER

ACTIVE OR LEAST NOBLE	
	Magnesium Magnesium Alloys Zinc Galvanized Steel
	Aluminum 1100
	Aluminum 6053 Alclad
	Cadmium
	Aluminum 2024 (4.5 Cu, 1.5 Mg 0.6 Mn)
	Mild Steel Wrought Iron Cast Iron
	13% Chromium Stainless Steel Type 410 (Active)
	18-8 Stainless Steel Type 304 (Active)
	18-12-3 Stainless Steel Type 316 (Active)
	Lead-Tin Solders Lead Tin
	Manganese Bronze Naval Brass
	Nickel (Active) 76 Ni - 16 Cr - 7 Fe Alloy (Active)
	60 Ni - 30 Mo - 6 Fe - 1 Mn
	Yellow Brass Admiralty Brass Aluminum Brass Red Brass Copper Silicon Bronze
	70:30 Cupro Nickel G-Bronze M-Bronze Silver Solder Nickel (Passive) 76 Ni - 16 Cr - 7 Fe Alloy (Passive) 67 Ni - 33 Cu Alloy (Monel)
	13% Chromium Stainless Steel Type 410 (Passive) Titanium
	18-8 Stainless Steel Type 304 (Passive) 18-12-3 Stainless Steel Type 316 (Passive)
	Silver
	Graphite Gold Platinum
PASSIVE OR MORE NOBLE	

Corrosion Guide

The sheath materials in the following tables are to be used as a guide only and not as a firm recommendation. Such factors as temperature of solution, percentage of concentration, watt density and contamination are all factors in corrosion rates which make it impossible to make an absolute recommendation. For further information on corrosiveness of a solution, check the supplier of your solution.

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WARNING: Certain solutions, due to their viscosity or flammability are not suitable for heating with direct immersion heaters unless special precautions are taken. Check factory if you require assistance in the selection of a safe and reliable heating method for your application.

LEGEND: A - GOOD
 F - FAIR
 C - DEPENDS ON CONDITIONS
 X - UNSUITABLE

SOLUTION	IRON AND STEEL	300 SERIES STAINLESS	MONEL	INCOLOY	INCONEL	COPPER	TITANIUM	ALUMINIUM QUARTZ	TEFLON
Acetaldehyde		A-316				A			
Acetic Acid, Crude	X	F	F	C	C	F	F		
Pure			A	C	C	F	F	A	
Vapors			F	C	C	F	F	C	
150 PSI; 400°F			F	C	C	F	F	C	
Aerated	X	F-316 X-304	X	X	X	A	C		
No Air		C	A	X	F	A	C		
Acetone	C	A	A	A	A	A	F	A	
Alboloy Process	A								
Allyl Alcohol		A	A	A	A	A	F		
Alcohol	F	A-316	A	A	A	A	F	A	
Alkaline Solutions	A	A-304							
Alkaline Cleaners		A-304							X
Alkaline Soaking Cleaners	A								
Alum									
Aluminum (molten)									
Aluminum Acetate	X	A-316	F		F	F	A		
Aluminum Bright Dip									A A
Aluminum Chloride	X	X	X	X	X	X	X	X	A A
Aluminum Cleaners	C	A	A	A	A	X	F	X	X
Aluminum Potassium Sulphate (Alum)		C-316 X-304	F		F	A	F	X	
Aluminum Sulphate	X	F	F	X	X	F	A	X	A
Ammonia	X	X	X	C	F	X	A	C	A
Ammonia Gas, Cold	A	A	A		A	C	A	A	
Hot	C	C	C		A	X			
Ammonia and Oil	A								
Ammonium Acetate	A	A	A	A	A	X		A	
Ammonium Bifluoride	X	X	X	X	X	X	X	X	A
Ammonium Chloride	C	F	F	C	C	X	A	X	A A
Ammonium Hydroxide	A	A	C	A	A	X	A	C	X

SOLUTION	IRON AND STEEL	300 SERIES STAINLESS	MONEL	INCOLOY	INCONEL	COPPER	TITANIUM	ALUMINIUM QUARTZ	TEFLON
Ammonium Nitrate	A	A	C	X	X	X	X	F	A
Ammonium Persulphate	X	F	X		X	X		X	A A
Ammonium Sulphate	A	A	A	F	F	F	A	X	A
Anhydrous Ammonia	A					X			
Aniline	F	A	F	F	F	X	A	F	A
Aniline, Aniline Oil	A	A	A	F	F	X	A	X	A
Aniline, Dyes		A	A						
Anodizing Solutions 10%									
Chromic Acid 96°F	C	A					A		
Sodium Hydroxide Alkaline	A			A			A		
Nickel Acetate			A						
Arsenic Acid	X	C	X	X	X	X	X	X	A A
Asphalt	A	A	X	A	A	X	A	X	A
Barium Chloride		F-304 X-316			A			X	
Barium Hydroxide		A		F	F	X	X	X	A
Barium Sulphate	F	F	F	F	F	F	A		A
Barium Sulphide		A	A			X			
Barium Sulphite		F-304							
Black Nickel									A A
Black Oxide		A-304							
Bonderizing	C	A		C	C		A		A A
Boric Acid	X	C	C	C	C	C	A	X	A A
Brass Cyanide		A-304							
Bright Nickel							A		A
Brine (Salt Water)			A		F				
Bronze Plating	A	A-304							
Butanol (Butyl Alcohol)	A	A	A	A	A	A	A	F	A A
Cadmium Black									A
Cadmium Fluoborate									A
Cadmium Plating				A	A				
Calcium Chlorate	F	F	F	F	F	C			A
Calcium Chloride	F	F	F	F	F	F	A	C	A A
Carbolic Acid, Phenol	C	A	A	F	F	X	A	F	
Carbon Dioxide, Dry	A	A	A	A	A	A	X	A	A X
Wet	F	A	A	A	A	F	X	A	A X
Carbon Tetrachloride	C	C	A	A	A	C	A	X	A
Carbonic Acid	C	A-304	C	F	A	C	A	C	A A
Castor Oil	A	A	A	A	A	A	A	A	A A
Caustic Etch	A	A	A	X	X	X	A	X	A X
Caustic Soda (Lye) (Sodium Hydroxide)	X	C-316 X-304	C	C	F	X	C	X	X A
2%	F	F-316 X-304	A	A	A	F	A	X	
10 - 30%, 210°F	F	A	A	A	A	F	A	X	
76%, 180°F	X	F	F	A	A	X	F	X	
Chlorine, Dry	A	A	A	C	F	A	F	X	A F
Wet	X	X	X	X	X	X	X	X	A X
Chloroacetic Acid	X	X		C	C	X	A	X	A A
Chromic Acetate									A
Chromic Acid	C	A	F	X	X	X	A	X	A X
Chrome Plating				X	X		A		A X
Citric Acid	X	A	A	F	F	A	A	C	A A
Clear Chromate		A-316							
Cobalt Acetate 130°F			A	F	F				
Cobalt Nickel									A
Cobalt Plating		A-304							A
Coconut Oil			F						
Cod Liver Oil		A		A	A			A	
Copper Acid							A		A

Corrosion Guide (continued)

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SOLUTION	IRON AND STEEL	300 SERIES STAINLESS	MONEL	INCOLOY	INCONEL	COPPER	TITANIUM	ALUMINIUM	QUARTZ	TEFLON
Copper Bright		A								
Copper Bright Acid								A		
Copper Chloride	F	X	F	X	X	C	A	C	A	A
Copper Cyanide	A			X	X			X	A	A
Copper Fluoborate		F	F	F	F					A
Copper Nitrate	X	F	X	X	X	X		X	A	A
Copper Plating	A									
Copper Sulphate	X	A	A	F	F	C		X	A	
Creosote	A	A	A	F	F	A		C	A	
Deionized Water	X	A	A	A	A	X		X		
Deoxidine		A								
Deoxidizer (Etching)										A
Diethylene Glycol	F	A	F	F	F	F	A	F	A	A
Diphenyl 300°-350°	A				A			A		
Disodium Phosphate 25% 180°F	A				A			A	A	
Dowtherm A	A			A						
Electro Polishing										A
Electroless Nickel								A	A	
Electroless Tin (Acid)										A
(Alkaline)		A-316						A		
Ethers	A		A	F	F	A	A	F	A	
Ethyl Chloride	A	A	A	F	A	A	A	F	A	A
Ethylene Glycol 300°F		A	A	F	F			A	A	A
Fatty Acids	X	A-316	F	F	F	X	A	A	A	
Ferric Chloride	X	X	X	X	X	X	A	X	A	A
Ferric Nitrate	X	F	X	X	X	X		X	A	
Ferric Sulphate	X	F-304 A-316	X	C	C	X	A	X	A	
Fluorine Gas, Dry	C	C	A	C	A	X	A	X	C	
Formaldehyde	F	A	A	F	F	F	A	F	A	

SOLUTION	IRON AND STEEL	300 SERIES STAINLESS	MONEL	INCOLOY	INCONEL	COPPER	TITANIUM	ALUMINIUM	QUARTZ	TEFLON
Formic Acid	X	F	C	F	C	F	X	X	A	
Freon	C	C	A	A	A	A		A		
Fuel Oil	A	A	A	F	F	A	A	A		
Fuel Oil, Acid	C	C	A	C	C	C	A	X		
Gasoline, Refined	A	A	A	F	F	A		A	A	
Gasoline, Sour	C	A	A	X	X	C		C	A	
Glycerine, Glycerol	A	A	A	A	A	F		A	A	
Gold - Acid	A						A		A	
Gold - Cyanide		A								
Grey Nickel							A		A	A
Hydrochloric Acid <150°F	X	X	C	X	X	X	X	X	A	
>150°F	X	X	C	X	X	X	X	X	A	A
Hydrocyanic Acid (No Air)	X	F	F	F	F	X		F	A	
Hydrofluoric Acid, Cold <65%	X	X	F	X	X	C	X	X	X	A
>65%	F	X	A	X	X	F	X	X		
Hot <65%	X	X	C				X	X		
>65%	C	X	A	X	X	F	X	X		
Hydrogen Peroxide	X	A	F	F	F	X	A	A	A	
Indium									A	A
Iron Phosphate (Parkerizing)	C	A								
Isopropanol	C		A		A	F				
Kerosene	A	A	A	A	A	A		A		
Lacquer Solvents	C	A	A	F	F	C	A	A	A	
Lard	F									
Lead Acetate	X	A	A	A	A	X	A	X	A	
Lead Acid Salts		A-304								
Lime Saturated Water	F	A-316	F	F	F	F		X	X	
Linseed Oil	A	A	A	F	F	A	A	F		
Magnesium Chloride	F	F	F	F	A	F	A	X	A	
Magnesium Hydroxide	A	A	A	A	A	X		F	A	
Magnesium Nitrate	F	F	F	F	X	F	F	F	A	
Magnesium Sulphate	A	A	A	F	A	A	A	F	A	
Mercuric Chloride	C	X	X	X	X	X	F	X	A	
Mercury	A	A	A	A	F	X	X	X	A	
Methyl Alcohol, Methanol	A	A	A	F	A	A	A	C	A	
Methyl Bromide	C	A	F	F	F	F	A	X	A	
Methyl Chloride	A		A	C	C	A	A	X	A	
Methylene Chloride	X	C	C	C	F	C	A	C	A	
Mineral Oils	A	A	A	A	A	A	A	A	A	
Muriato									A	A
Naptha	A	A	A	A	A	A	A	A	A	A
Napthalene	A			F	F		A	F		
Nickel Acetate Seal		A-316								
Nickel Chloride		F	C	C	F	X	F	X	A	A
Nickel Copper Strike (Cyanide Free)		A								
Nickel Plating, Bright								A	A	A
Nickel Plating, Dull									A	A
Nickel Plating, Watts Solution								A	A	A
Nickel Sulphate	X	A	C	C	C	X		X	A	A
Nitric Acid, Crude	X	C	X	X	X	X		X	A	A
Concentrated	X	F	X	X	X	X		X	A	A
Diluted	X	A	X	X	X	X		X	A	A
Nitric Hydrochloric Acid	X	X	X	X	X	X	X	X	A	A
Nitric 6% Phosphoric Acid		C-316							A	A
Nitric Sodium Chromate		A-316							A	A
Nitrobenzene	A	A	A	A	A	F	A	A	A	
Oakite No. 20	A									
Oakite No. 23	A									
Oakite No. 24	A									

SOLUTION	IRON AND STEEL	300 SERIES STAINLESS	MONEL	INCOLOY	INCONEL	COPPER	TITANIUM	ALUMINUM	QUARTZ	TEFLON
Oakite No. 30	A									
Oakite No. 51	A									
Oakite No. 67		A-304								
Oakite No. 90 @ 180°F	A									
Oleic Acid	C	A	A	F	A	X	F	C	A	A
Oxalic Acid	C	C	A	X	F	C	X	F	A	A
Paint Stripper (High Alkaline Type)	A									
Paint Stripper (Solvent Type)		A-316								
Paraffin	A	A				A		A		
Parkerizing										
Perchloroethylene		A		F	A		A	C	A	
Petroleum Oils, Crude <500°F	A	A	C	A		C		A	A	
>500°F	A	A	X			X		A		
>1000°F	X	C	X			X		X		
Phenol		A-347								
Phenol 85%, 120°F	C	A		F	F		A	A		
Phosphate		A-316								X
Phosphate Cleaner		A-304								X
Phosphatizing		A-316								X
Phosphoric Acid, Crude	C	C	X			X		X		
Pure <45%	X	A	F	A	A	F	X	C		
>45% Cold	X	A	F	A		F	X	X		
Hot	X	X-304 C-316	C	A	F	C	X	X		
Photo Fixing Bath		A	C							
Potassium Bichromate (Potassium Dichromate)	C	A-316	F	F		F	F	A	A	
Potassium Chloride	A	A	A	C	F	A	A	X	A	
Potassium Cyanide	A	A	A	F	F	X	X	X	A	A
Potassium Hydrochloride									A	A
Potassium Hydroxide	C	F	A	C	F	X	X	X	X	A
Potassium Nitrate (Salt Peter)	F	F	F	F	F	F	A	A	A	
Potassium Sulphate	A	F	A	F	F	A	A	A	A	A
Prestone 350°F	A		A							
Sea Water	X	C	A	F	F	X	A	X	A	
Silver Bromide	X	X	C			X	A	X	A	A
Silver Cyanide	C	A	F	A		X	X	X	A	
Silver Nitrate	X	C	X	C	C	X	A	X	A	
Soap Solutions	A	A	A			C		X		
Sodium - Liquid Metal	C	A-304	C	A	A	X		X	X	
Sodium Bisulphate	X	X	C		F	F		C		
Sodium Bromide	F	C	F	F	F	F		X	A	A
Sodium Carbonate <20%	A			F	F		A	X	C	A
Sodium Chlorate	X	F	A	F	A	A	A	F	A	A
Sodium Chloride	A	F-304 A-316	A	F	A	F	C	X	A	
Sodium Citrate	X	F				X		X	A	A
Sodium Cyanide	A	A-316	F	A	A	X	C	X	A	
Sodium Dichromate (Sodium Bichromate)	F	F				X	C	C	A	
Sodium Disulphate	X	X	C		C		C	C	A	
Sodium Hydroxide	A	F	A	A	A	X	A			
Sodium Hypochlorite	X	X	C	X	X	C	A	X	A	A
Sodium Nitrate	A	F-304 A-316	A	A	A	F	A	C	A	
Sodium Peroxide	C	A	A		F			C		
Sodium Phosphate	C	A-316	A	F	A	F	A	X	A	A
Sodium Salicylate	F	F	F	F	F	F			A	A
Sodium Silicate	A	A-316	A	F	F	C		X	A	A

SOLUTION	IRON AND STEEL	300 SERIES STAINLESS	MONEL	INCOLOY	INCONEL	COPPER	TITANIUM	ALUMINUM	QUARTZ	TEFLON
Sodium Stannate	C	F	F	F	F				A	A
Sodium Sulphate	A	A	A	F	F	A	C	F	A	A
Sodium Sulphide	A	A	F	C	C	X	C	C	C	A
Solder Bath	X	X	X	X	X	X	X	X	X	X
Soybean Oil		A								
Steam <500°F	A	A	A	A	A	A				
500-1000°F	C	A	C	A	A	C				
>1000°F	X	A	X	A	A	X				
Stearic Acid	C	A	A			C		C	A	
Sugar Solution	A	A	A	A	A	A	A	A	A	A
Sulphur	A	F	X	A	A	X	A	A	A	
Sulphur Chloride	X	C-304 X-316	X	C	F	X		X	A	A
Sulphur Dioxide	C	C	X	C	C	C	A	C	A	
Sulphuric Acid <10% Cold	X	F	C		X	C		C		
Hot	X	F-316 X-304	C		F	X		C		
10-75% Cold	X	X-304 F-316	C		X	X	X	X		
Hot	X	X	C		X	X	X	X		
75-95% Cold	C	A	C		X	X	X	X		
Hot	F	X	C		X	X	X			
Fuming	C	C-304 F-316	X	C	C	X		X		
Sulphurous Acid	A	C-316 X-304	X		C	C	A	C		
Tannic Acid		F	A		A	A	A	C	A	
Tar	A	A		A	A			A		
Tartaric Acid		C-304 A-316	C		F	F	F	C		
Tetrachlorethylene	A			F	A		A	C	A	
Thermoil Granodine	F									
Tin (Molten)	F	F	X		X	X	A	X		X
Tin-Nickel Plating									A	A
Tin Plating - Acid										A
Tin Plating - Alkaline	A	A-304								
Toluene	A	A	A	A	A	C	A	A		
Triad Solvent	C									
Trichloroethane	A	A-304	F	F	F	F	A	F	A	
Trichloroethylene	C	C	A	A	A	C	A	F	A	
Triethylene Glycol	A	A	A	A	A	A	A	A		
Trioxide (Pickle)									A	A
Trisodium Phosphate	A	C	C			C		X	X	X
Turpentine	C	A	A			C		A		
Urea Ammonia Liquor 48°F	A									
Vegetable Oil	C	A	A	A		X		F		
Vinegar	C	F-304 A-316	A					C		
Water, Fresh	C	A	A	A	A	A	A	A		A
Distilled, Lab Grade	X	A	C	A	A	X				
Return Condensate	A	A	A	A	A	A				
Whiskey and Wines	X	F-304 A-316	A	A	A	A				
Yellow Dichromate		A-316							A	
X-Ray Solution		A								
Zinc (Molten)		X	X	X	X	X	X	X		X
Zinc Chloride	C	X	A	F	F	X	F	X	A	A
Zinc Plating Acid									A	
Zinc Plating Cyanide	A	A-304								
Zinc Sulphate	C	A	A	A	A	X	A	C		

Typical Watt Densities

1. Watt density is determined by dividing the heater wattage by the total surface area of all heated surfaces on the element. Remember that electric heating elements will continue to increase their surface temperature until all heat produced by the element is transferred to the work.
2. Typical watt densities shown in the table below are based on non-circulated liquids unless noted otherwise.

MATERIAL BEING HEATED	MAXIMUM WATTS PER SQUARE INCH	OPERATING TEMP. (°F)	
Acetaldehyde	14	180	
Acetone	14	130	
Acid Solutions (Mild)	Acetic	40	180
	Boric	40	257
	Carbonic	40	180
	Chromic	40	180
	Citric	25	180
	Fatty Acids	25	150
	Lactic	10	122
	Malic	14	120
	Nitric	25	167
	Phenol - 2-4 Disulfonic	40	180
	Phosphoric	28	180
	Phosphoric (Aerated)	26	180
Proponic	40	180	
Tannic	30 / 40	160 / 180	
Alkaline Solutions	44	212	
Aluminum Acetate	14	122	
Aluminum Potassium Sulfate	40	212	
Ammonium Acetate	28	167	
Amyl Acetate	28	240	
Amyl Alcohol	24	212	
Aniline	26	350	
Asphalt	4 - 10	200 - 500	
Barium Hydroxide	40	212	
Benzene, liquid	14	150	
Butyl Acetate	14	225	
Calcium Bisulfate	20	400	
Calcium Chloride	5 - 8	200	
Carbon Monoxide	25	—	
Carbon Tetrachloride	25	160	
Caustic Soda	2%	50	210
	10%	28	210
	75%	26	180
Citrus Juices	26	185	
Degreasing Solution	25	275	
Dextrose	25	212	
Dowtherm A	1 ft. sec. or more non-flowing	23	750
		10	750
Dowtherm E	12 - 18	400	
Dyes & Pigments	23	212	
Electroplating Baths	Cadmium	40	180
	Copper	40	180
	Dilute Cyanide	40	180
	Sodium Cyanide	40	180
	Potassium Cyanide	40	180
Ethylene Glycol	30	300	
Formaldehyde	12	180	
Freon gas	2 - 5	300	
Fuel Oils	Grades 1 & 2 (distilate)	23	200
	Grades 4 & 5 (residual)	14	200

3. Use of watt density lower than listed will prolong heater service life.
4. This data is for use as a general guideline only. System conditions may exist that may mandate densities lower or higher than listed. Certain substances of high viscosity and low heat transfer may be subject to coking if density is too high.

MATERIAL BEING HEATED	MAXIMUM WATTS PER SQUARE INCH	OPERATING TEMP. (°F)	
Fuel Oils	Grades 6 & bunker C (residual)	8	160
Gasoline		25	300
Gelatin	Liquid	25	150
	Solid	6	150
Glycerine		10	500
Glycerol		26	212
Grease	Liquid	26	—
	Solid	5	—
Heat Transfer Oils	Static	18	500
		14	600
	Circulating	24	500
		22	600
Hydrazine	18	212	
Linseed Oil	50	150	
Lubrication Oil	SAE 10	26	250
	SAE 20	24	250
	SAE 30	23	250
	SAE 40	16	250
	SAE 50	14	250
Magnesium Chloride	40	212	
Magnesium Sulfate	40	212	
Manganese Sulfate	40	212	
Methylamine	22	180	
Methylchloride	20	180	
Mineral Oil	25	200	
	18	400	
Molasses	5	100	
Molten Salt Bath	25 - 30	800 - 900	
Naptha	12	212	
Oil Draw Bath	25	600	
Paraffin or Wax (liquid state)	20	150	
Perchloroethylene	25	200	
Potassium Chlorate	40	212	
Potassium Chloride	40	212	
Potassium Hydroxide	23	160	
Soap, liquid	24	212	
Sodium Acetate	45	212	
Sodium Cyanide	45	140	
Sodium Hydride	30	720	
Sodium Hydroxide			
Sodium Phosphate	40	212	
Sulfur, Molten	10	600	
Therminols	26	500	
	23	600	
	15	650	
Toluene	25	212	
Trichlorethylene	25	150	
Turpentine	22	300	
Vegetable Oil & Shortening	40	400	
Water (Process)	60 - 90	212	

PRACTICAL FLOW VELOCITIES IN PIPE

FLOW/SERVICE	PSIG	VELOCITY
Saturated Steam	0-25	4000-6000 ft./min.
	25 and up	6000-10000 ft./min.
Superheated Steam	200 and up	7000-20000 ft./min.
Water/Boiler Feed	-	8 - 15 ft./sec.
Water/Pump Suction	-	4 - 7 ft./sec.
Water/Drain	-	4 - 7 ft./sec.
Water/General Service	-	4 - 10 ft./sec.

ALLOWABLE PRESSURE RATINGS FOR PIPES AND FLANGES

The information included on this page is to be used as a guide only in the pre-selection of pipe and flange sizes for various temperatures and pressures.

When calculating thickness requirements in accordance with the ASME code for safe pressure vessel design, stress values may often be less than shown in Table 1.

TABLE 1 - APPROXIMATE ALLOWABLE STRESS FOR PIPE IN PSIG

TEMP. °F	PIPE MATERIAL AND TYPE			
	A53B WELDED STEEL	A106B SEAMLESS STEEL	A312 304 S.S. WELDED	A312 316 S.S. WELDED
100	14,600	17,100	17,000	17,000
300	14,600	17,100	16,100	17,000
500	14,600	17,100	14,800	15,300
650	14,600	17,100	13,800	14,100
700	13,300	15,600	13,500	13,900
900	5,000	5,900	12,400	13,200
1100	-	-	8,300	10,500
1300	-	-	3,100	3,500

DETERMINATION OF APPROXIMATE PIPE WALL THICKNESS (t_N) FOR VARIOUS PRESSURES AND TEMPERATURES

$$t_N = \frac{.5PD}{SE - .6P} \quad (1.143)$$

t_N = Nominal pipe wall thickness (page D48) not including corrosion allowance

P = Max. pressure (PSIG)

D = Inside pipe diameter (in.)

S = Allowable stress from Table 1

E = Joint efficiency (assume a value of 1.0 for seamless pipe or welded pipe where full radiography is done).

FLANGE PRESSURE - TEMPERATURE RATINGS

METAL	MAX. ALLOWABLE PRESSURE (PSIG)						
	TEMP. °F	150 LB.	300 LB.	400 LB.	600 LB.	900 LB.	1500 LB.
CARBON STEEL	100	285	740	990	1480	2220	3705
	200	260	675	900	1350	2025	3375
	300	230	655	875	1315	1970	3280
	400	200	635	845	1270	1900	3170
	500	170	600	800	1200	1795	2995
	600	140	550	730	1095	1640	2735
	650	125	535	715	1075	1610	2685
	700	110	535	710	1065	1600	2665
	750	95	505	670	1010	1510	2520
	800	80	410	550	825	1235	2060
304 S.S.	100	275	720	960	1440	2160	3600
	200	235	600	800	1200	1800	3000
	300	205	540	720	1080	1620	2700
	400	190	495	660	995	1490	2485
	500	170	465	620	930	1395	2330
	600	140	435	580	875	1310	2185
	700	110	425	565	850	1275	2125
	800	80	405	540	805	1210	2015
	900	50	390	520	780	1165	1945
	1000	20	320	430	640	965	1605
316 S.S.	100	275	720	960	1440	2160	3600
	200	235	620	825	1240	1860	3095
	300	215	560	745	1120	1680	2795
	400	195	515	685	1030	1540	2570
	500	170	480	635	955	1435	2390
	600	140	450	600	900	1355	2255
	700	110	430	580	870	1305	2170
	800	80	420	565	845	1265	2110
	900	50	415	555	830	1245	2075
	1000	20	350	465	700	1050	1750
304L 316L S.S.	100	230	600	800	1200	1800	3000
	200	195	505	675	1015	1520	2530
	300	175	455	605	910	1360	2270
	400	160	415	550	825	1240	2065
	500	145	380	510	765	1145	1910
	600	140	360	480	720	1080	1800
	700	110	345	460	685	1030	1715
	800	80	330	440	660	985	1645

REFERENCE ASME/ANSI B16.5 - 1998

TABLE 1 - Sheet metal gauges in approximate decimals of an inch

No. of Sheet Metal Gauge	Manufacturers' Standard Gauge for Steel		300 Series Stainless Steel		Galvanized Sheet Steel Thk.
	Thk.	lbs./ft ²	Thk.	lbs./ft ²	
9	0.1495	6.2500	—	—	0.1532
10	0.1345	5.6250	0.134	5.628	0.1382
11	0.1196	5.0000	0.119	4.998	0.1233
12	0.1046	4.3750	0.103	4.326	0.1084
13	0.0897	3.7500	—	—	0.0934
14	0.0747	3.1250	0.074	3.108	0.0785
15	0.0673	2.8125	—	—	0.0710
16	0.0598	2.5000	0.059	2.478	0.0635
17	0.0538	2.2500	—	—	0.0575
18	0.0478	2.0000	0.047	1.974	0.0516
19	0.0418	1.7500	—	—	0.0456
20	0.0359	1.5000	0.035	1.470	0.0396
21	0.0329	1.3750	—	—	0.0366
22	0.0299	1.2500	0.030	1.260	0.0336
23	0.0269	1.1250	—	—	0.0306
24	0.0239	1.0000	0.024	1.008	0.0276
25	0.0209	0.87500	—	—	0.0247
26	0.0179	0.75000	0.019	0.798	0.0217
27	0.0164	0.68750	—	—	0.0202
28	0.0149	0.62500	—	—	0.0187
29	0.0135	0.56250	—	—	0.0172
30	0.0120	0.50000	—	—	0.0157
31	0.0105	0.43750	—	—	0.0142
32	0.0097	0.40625	—	—	0.0134
33	0.0090	0.37500	—	—	—
34	0.0082	0.34375	—	—	—
35	0.0075	0.31250	—	—	—
36	0.0067	0.28125	—	—	—

TABLE 2 - 80-20 NiCr wire properties (650 ohms circ. mil/ft)

B & S	DIAM. (INS.)	OHMS/FT (77°F)	B & S	DIAM. (INS.)	OHMS/FT (77°F)
13	.072	0.125	25	.0179	2.029
14	.064	0.158	26	.0159	2.571
15	.057	0.200	27	.0142	3.224
16	.051	0.250	28	.0126	4.094
17	.045	0.321	29	.0113	5.090
18	.040	0.406	30	.0100	6.500
19	.036	0.501	31	.0089	8.206
20	.032	0.635	32	.0080	10.160
21	.0285	0.800	33	.0071	12.890
22	.0253	1.015	34	.0063	16.330
23	.0226	1.273	35	.0056	20.730
24	.0201	1.609	36	.0050	26.000

TABLE 3 - DIMENSIONS OF STEEL PIPE

DIAMETER IN INCHES NOMINAL (O.D.)	SCHEDULE NO.	WALL THICKNESS INCHES	DIAMETER IN INCHES NOMINAL (O.D.)	SCHEDULE NO.	WALL THICKNESS INCHES
1/8 (0.405)	10S	0.049	6 (6.625)	5S	.109
	40ST, 40S	.068		10S	.134
	80XS, 80S	.095		40ST, 40S	.280
1/4 (0.54)	10S	.065	8 (8.625)	5S	.109
	40ST, 40S	.088		10S	.148
	80XS, 80S	.119		20	.250
3/8 (0.675)	10S	.065	10 (10.75)	5S	.134
	40ST, 40S	.091		10S	.165
	80XS, 80S	.126		20	.250
1/2 (0.84)	5S	.065	12 (12.75)	5S	0.156
	10S	.083		10S	0.180
	40ST, 40S	.109		20	0.250
	80XS, 80S	.147		30	0.330
	160	.188		40	0.406
3/4 (1.05)	5S	.065	14 (14)	5S	0.156
	10S	.083		10S	0.188
	40ST, 40S	.113		10	0.250
	80XS, 80S	.154		20	0.312
	160	.219		30, ST	0.375
1 (1.315)	5S	.065	16 (16)	5S	0.165
	10S	.109		10S	0.188
	40ST, 40S	.133		10	0.250
	80XS, 80S	.179		20	0.312
	160	.250		30, ST	0.375
1 1/4 (1.66)	5S	.065	18 (18)	5S	0.165
	10S	.109		10S	0.188
	40ST, 40S	.140		10	0.250
	80XS, 80S	.191		20	0.312
	160	.250		30, ST	0.375
1 1/2 (1.9)	5S	.065	20 (20)	5S	0.165
	10S	.109		10S	0.188
	40ST, 40S	.145		10	0.250
	80XS, 80S	.200		20	0.312
	160	.281		30, ST	0.375
2 (2.375)	5S	.065	24 (24)	5S	0.165
	10S	.109		10S	0.188
	40ST, 40S	.154		10	0.250
	80ST, 80S	.218		20	0.312
	160	.344		30, ST	0.375
2 1/2 (2.875)	5S	.083	30 (30)	5S	0.165
	10S	.120		10S	0.188
	40ST, 40S	.203		10	0.250
	80XS, 80S	.276		20	0.312
	160	.375		30, ST	0.375
3 (3.5)	5S	.083	36 (36)	5S	0.165
	10S	.120		10S	0.188
	40ST, 40S	.216		10	0.250
	80SX, 80S	.300		20	0.312
	160	.438		30, ST	0.375
3 1/2 (4.0)	5S	.083	42 (42)	5S	0.165
	10S	.120		10S	0.188
	40ST, 40S	.226		10	0.250
	80XS, 80S	.318		20	0.312
	160	.531		30, ST	0.375
4 (4.5)	5S	.083	48 (48)	5S	0.165
	10S	.120		10S	0.188
	40ST, 40S	.237		10	0.250
	80SX, 80S	.337		20	0.312
	120	.438		30, ST	0.375
5 (5.563)	5S	.109	60 (60)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
6 (6.625)	5S	.109	72 (72)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
8 (8.625)	5S	.109	84 (84)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
10 (10.75)	5S	.109	96 (96)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
12 (12.75)	5S	.109	108 (108)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
14 (14)	5S	.109	120 (120)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
16 (16)	5S	.109	144 (144)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
18 (18)	5S	.109	168 (168)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
20 (20)	5S	.109	192 (192)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
24 (24)	5S	.109	216 (216)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
30 (30)	5S	.109	252 (252)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
36 (36)	5S	.109	288 (288)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
42 (42)	5S	.109	336 (336)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
48 (48)	5S	.109	396 (396)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
60 (60)	5S	.109	474 (474)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
72 (72)	5S	.109	564 (564)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
84 (84)	5S	.109	660 (660)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
96 (96)	5S	.109	768 (768)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
108 (108)	5S	.109	888 (888)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
120 (120)	5S	.109	1032 (1032)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
144 (144)	5S	.109	1200 (1200)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
168 (168)	5S	.109	1404 (1404)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
192 (192)	5S	.109	1632 (1632)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S	.258		10	0.250
	80XS, 80S	.375		20	0.312
	120	.500		30, ST	0.375
216 (216)	5S	.109	1872 (1872)	5S	0.165
	10S	.134		10S	0.188
	40ST, 40S				

Atmospheric Conditions and Temperature Codes

The information listed on this page is to be used only as a general guide. Consult the latest edition of the Code to check the suitability of the explosion-proof heater to your needs.

For detailed information concerning the installation of electrical equipment in hazardous locations, refer to either the Canadian Electrical Code Part 1 Section 18, available from the Canadian Standards Association, or the National Electrical Code Chapter 5 Articles 500 through 503, available from the National Fire Protection Association.

Where electrical equipment is required by Section 18 or Chapter 5 to be approved for the class of location, it shall also be approved for the specific gas, vapour, or dust that will be present. Such approval may be indicated by one or more atmospheric group designations which have been established for the purpose of testing and approval.

Note that the maximum external temperature of the equipment shall not exceed the minimum ignition temperature of the atmosphere as listed in Table 2.

For example:

Assume the maximum heater temperature is listed as T2C or 230°C (446°F). This heater would not be suitable for use in atmospheres containing octanes but would be suitable for use in atmospheres containing gasoline.

For octanes, select a heater having a temperature code that does not exceed 206°C (403°F).

TABLE 1 - Equipment Maximum Temperature

Temperature Code	Maximum External Temperature
T1	450°C / 842°F
T2	300°C / 572°F
T2A	280°C / 536°F
T2B	260°C / 500°F
T2C	230°C / 446°F
T2D	215°C / 419°F
T3	200°C / 392°F
T3A	180°C / 356°F
T3B	165°C / 329°F
T3C	160°C / 320°F
T4	135°C / 275°F
T4A	120°C / 248°F
T5	100°C / 212°F
T6	85°C / 185°F

TABLE 2 - Atmospheric Conditions

ATMOSPHERE	MIN. IGNITION TEMP. LIMIT
GROUP A CONTAINING acetylene	305°C / 581°F
GROUP B CONTAINING butadiene ethylene oxide hydrogen manufactured gases containing more than 30% hydrogen (by volume) propylene oxide	420°C / 788°F 429°C / 804°F 500°C / 932°F 500°C / 932°F 499°C / 930°F
GROUP C CONTAINING acetaldehyde cyclopropane diethyl ether ethylene unsymmetrical dimethyl hydrazine (UDMH 1, 1-dimethyl hydrazine)	175°C / 347°F 498°C / 928°F 160°C / 320°F 450°C / 842°F 249°C / 480°F
GROUP D CONTAINING acetone acrylonitrile alcohol (see ethyl alcohol) ammonia benzene benzine (see petroleum naphtha) benzol (see benzene) butane 1-butanol (butyl alcohol) 2-butanol (secondary butyl alcohol) butyl acetate isobutyl acetate ethane ethanol (ethyl alcohol) ethyl acetate ethylene dichloride gasoline heptanes hexanes isoprene methane methanol (methyl alcohol) 3-methyl-1-butanol (isoamyl alcohol) methyl ethyl ketone methyl isobutyl ketone 2-methyl-1-propanol (isobutyl alcohol) 2-methyl-2-propanol (tertiary butyl alcohol) naphtha (see petroleum naphtha) natural gas octanes pentanes 1-pentanol (amyl alcohol) petroleum naphtha propane 1-propanol (propyl alcohol) 2-propanol (isopropyl alcohol) propylene styrene toluene vinyl acetate vinyl chloride xylenes	465°C / 869°F 481°C / 898°F 651°C / 1204°F 498°C / 928°F 287°C / 549°F 343°C / 649°F 405°C / 761°F 425°C / 797°F 421°C / 790°F 472°C / 882°F 363°C / 685°F 426°C / 799°F 413°C / 775°F 280°C / 536°F 204°C / 399°F 223°C / 433°F 395°C / 743°F 537°C / 999°F 385°C / 725°F 350°C / 662°F 404°C / 759°F 448°C / 838°F 415°C / 779°F 478°C / 892°F 482°C / 900°F 206°C / 403°F 260°C / 500°F 300°C / 572°F 288°C / 550°F 432°C / 810°F 412°C / 774°F 399°C / 750°F 455°C / 851°F 490°C / 914°F 480°C / 896°F 402°C / 756°F 472°C / 882°F 463°C / 865°F
GROUP E COMPRISING atmospheres containing metal dust, including aluminum, magnesium, and their commercial alloys, and other metals of similarly hazardous characteristics	
GROUP F COMPRISING atmospheres containing carbon black, coal, or coke dust	
GROUP G COMPRISING atmospheres containing flour, starch, or grain dust, and other dusts of similarly hazardous characteristics	

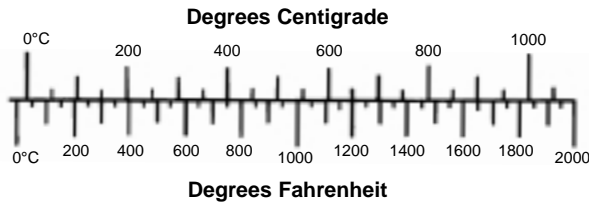
Temperature Conversion

$$^{\circ}\text{F} = 9/5^{\circ}\text{C} + 32$$

$$^{\circ}\text{R} = ^{\circ}\text{F} + 460$$

$$^{\circ}\text{C} = 5/9 (^{\circ}\text{F} - 32)$$

$$^{\circ}\text{K} = ^{\circ}\text{C} + 273$$



COMMON CONVERSION FACTORS

To Convert From	To	Multiply By
Atmospheres	mm Mercury (32°F)	760.
Atmospheres	Newtons / sq. meter	101,325.
Atmospheres	Ft. water (39.1°F)	33.90
Atmospheres	Ins. mercury (32°F)	29.921
Atmospheres	Pounds / sq. in.	14.696
Bars	Pounds / sq. in.	14.504
Boiler H.P.	Kilowatts	9.803
B.t.u.	Calories (gram)	252.
B.t.u. / hour	Watts	0.29307
B.t.u. / sec.	Watts	1,054.4
B.t.u. / sq. ft. / min.	Kilowatts / sq. ft.	0.1758
Circular mills	Square inches	7.854×10^{-7}
Cubic feet water	Pounds	62.37
Cubic feet / minute	Cubic cm / sec.	472.0
Cubic feet / minute	U.S. gallons / sec.	0.1247
Cubic feet / second	U.S. gallons / min.	448.8
Feet / min.	Miles / hour	0.011364
Gallons (U.S.)	Gallons (Imperial)	0.8327
H.P. (British)	Watts	745.7
Pounds	Grains	7,000.

SPECIAL CONVERSION FACTORS

To Convert From	To	Multiply By
Heat transfer		
p.c.u. / (hr.)(ft. ²)(°C)	B.t.u. / (hr.)(ft. ²)(°F)	1.
kg-cal. / (hr.)(m ²)(°C)	B.t.u. / (hr.)(ft. ²)(°F)	0.2048
g-cal. / (sec.)(cm ²)(°C)	B.t.u. / (hr.)(ft. ²)(°F)	7,380.
watts / (cm ²)(°C)	B.t.u. / (hr.)(ft. ²)(°F)	1,760.
watts / (in ²)(°F)	B.t.u. / (hr.)(ft. ²)(°F)	490.
B.t.u. / (hr.)(ft. ²)(°F)	p.c.u. / (hr.)(ft. ²)(°C)	1.
B.t.u. / (hr.)(ft. ²)(°F)	kg-cal. / (hr.)(m ²)(°C)	4.88
B.t.u. / (hr.)(ft. ²)(°F)	g-cal. / (sec.)(cm ²)(°C)	0.0001355
B.t.u. / (hr.)(ft. ²)(°F)	watts / (cm ²)(°C)	0.000568
B.t.u. / (hr.)(ft. ²)(°F)	watts / (in ²)(°F)	0.00204
B.t.u. / (hr.)(ft. ²)(°F)	hp / (ft. ²)(°F)	0.000394
B.t.u. / (hr.)(ft. ²)(°F)	joules / (sec.)(m ²)(°C)	5.678
kg-cal. / (hr.)(m ²)(°C)	joules / (sec.)(m ²)(°C)	1.163
watts / (m ²)(°C)	joules / (sec.)(m ²)(°C)	1.0

Viscosity

centipoises	g / (sec.)(cm) or poise	0.01
centipoises	lb. / (sec.)(ft.)	0.000672
centipoises	lb. / (hr.)(ft.)	2.42
centipoises	kg / (hr.)(m)	3.60
centipoises	(newton)(sec.) / m ²	0.001
lb. / (sec.)(ft.)	(newton)(sec.) / m ²	1.488

Thermal Conductivity

g-cal. / (sec.)(cm ²)(°C / cm)	B.t.u. / (hr.)(ft. ²)(°F / in.)	2903.0
watts / (cm ²)(°C / cm)	B.t.u. / (hr.)(ft. ²)(°F / in.)	694.0
g-cal. / (hr.)(cm ²)(°C / cm)	B.t.u. / (hr.)(ft. ²)(°F / in.)	0.8064
B.t.u. / (hr.)(ft. ²)(°F / ft.)	joules / (sec.)(m ²)(°C)	1.731
B.t.u. / (hr.)(ft. ²)(°F / in.)	joules / (sec.)(m ²)(°C)	0.1442

S. I. Conversions

BASIC CONVERSION FACTORS

Velocity		Power	
1 fps	= 0.3048 m/s	1 Btu/h(int.)	= 0.29307 W
1 fpm	= 0.00508 m/s	1 Btu/s(int.)	= 1.05506 kW
1 mph	= 0.44704 m/s	1 HP mech. (UK)	= 0.74570 kW
1 mph	= 1.60934 km/h	1 HP boiler	= 9.8095 kW
Length		Density	
1 inch	= 25.4 mm	1 lb./ft ³	= 16.01846 kg/m ³
1 foot	= 0.3048 m	1 lb./gal (imp.)	= 99.77633 kg/m ³
1 mile	= 1.60934 km	1 lb./gal (US)	= 119.82640 kg/m ³
Area		Thermal Conductivity	
1 sq. inch	= 6.4516 cm ²	1 Btu.ft/ft ² h.°F	= 1.73073 W/m ² °C
1 sq. foot	= 0.09290 m ²	1 Btu.in/ft ² h.°F	= 0.14423 W/m ² °C
Volume		Volumetric Flow	
1 inch ³	= 16.38706 cm ³	1 ft ³ /s	= 0.028317 m ³ /s
1 foot ³	= 0.02832 m ³	1 ft ³ /s	= 101.9406 m ³ /h
Capacity Imp. Measure		Kinematic Viscosity	
1 fluid oz.	= 28.41306 ml	1 ft ² /s	= 0.092903 m ² /s
1 gallon	= 4.54609 l	1 centistoke (cSt)	= 1.0 x 10 ⁻⁶ m ² /s
Weight or Mass		Dynamic Viscosity	
1 oz.	= 28.34952 g	1 centipoise (cP)	= 0.001 Pa-s
1 lb.	= 0.45359 kg	1 lb./ft.s	= 1.488164 Pa-s
Pressure		Heat Transfer	
1 psi	= 6.89476 kPa	1 Btu/ft ² h.°F	= 5.67826 W/m ² °C
1 bar	= 10 ⁵ Pa	1 kcal/m ² h.°F	= 1.163 W/m ² °C
Energy		Specific Energy	
1 kWh	= 3.6 MJ	1 Btu/lb.	= 2.326 kJ/kg
1 watt-hour	= 3.6 kJ	1 cal/g	= 4.1868 kJ/kg
Frequency		Specific Heat	
1 cps	= 1 Hz	1 Btu/lb.°F	= 4.1868 kJ/kg°C

DERIVED UNITS WITH SPECIAL NAMES

Measurement	Unit	Symbol	Derivation
Frequency	hertz	Hz	s ⁻¹
Force	newton	N	kg·m/s ²
Pressure	pascal	Pa	N/m ²
Energy	joule	J	N·m
Power	watt	W	J/s
Electric potential	volt	V	W/A
Electric resistance	ohm	Ω	V/A
Electric conductance	siemens	S	1/Ω
Electric charge	coulomb	C	A·s
Capacitance	farad	F	C/V
Magnetic flux	weber	Wb	V·s
Magnetic flux density	tesla	T	Wb/m ²
Inductance	henry	H	Wb/A
Luminous flux	lumen	lm	cd·sr
Illumination	lux	lx	lm/m ²
Temperature	Celsius degree	°C	K - 273.15
Pressure	bar	bar	10 ⁵ Pa
Volume	liter	l	dm ³

THE PREFERRED PREFIXES

Prefix	Symbol	Meaning	Prefix	Symbol	Meaning
tera-	T	10 ¹²	milli-	m	10 ⁻³
giga-	G	10 ⁹	micro-	μ	10 ⁻⁶
mega-	M	10 ⁶	nano-	n	10 ⁻⁹
kilo-	k	10 ³	pico-	p	10 ⁻¹²
deci-	d	10 ⁻¹	femto-	f	10 ⁻¹⁵
centi-	c	10 ⁻²	atto-	a	10 ⁻¹⁸